GEOTHERMAL GRADIENTS AND BURIAL HISTORY MODELLING IN PARTS OF THE EASTERN NIGER DELTA, NIGERIA

 $\mathbf{B}\mathbf{Y}$

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CERTIFICATION

ODUMODU, CHUKWUEMEKA FRANK, a Postgraduate student in the Department of Geology and with the Reg. No. PG/Ph.D/06/42148 has satisfactorily completed the requirements for course and research work for the degree of Ph.D in PETROLEUM GEOLOGY. The work embodied in this thesis is original and has not been submitted in part or in full for any diploma or degree of this or any other University.

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DEDICATION

This work is specially dedicated to my dear wife Phina and my lovely children, Kamso, Nonyelum, Ifeoma and Dimma.

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ABSTRACT

Reservoir and bottom hole temperatures from seventy wells in the Eastern Niger Delta suggests that two leg dogleg geothermal patterns characterize the geothermal gradients pattern of the Central Swamp and the Coastal Swamp in contrast to the single gradient patterns seen in the Shallow Offshore.

In the shallow/continental sections in the Niger Delta, geothermal gradients vary between 10 - 18 ° C/Km onshore, increasing to about 24 ° C/Km seawards. In the deeper (marine/parallic) section, geothermal gradients vary between 18 ó 45 °C/Km. The average geothermal gradient for the various depobelts is 19 °C/Km for the Central Swamp, 17°C/Km for the Coastal Swamp and 20°C/Km for the Shallow Offshore. Geothermal gradients in the Eastern Niger delta increase eastwards, northwards and seawards from the Coastal Swamp. Vertically, thermal gradients in the Niger Delta show a continuous and non-linear relationship with depth, increasing with diminishing sand percentages. As sand percentages decrease eastwards and seawards, thermal gradient increases. Thermal conductivies also decreases with depth from about 2.3 W/mK in the continental sands to 1.56 W/mK in the parallic and continuous shaly sections. Isothermals constructed at three depth levels: 1000m, 2000m, and 3000m shows that depressed temperatures occur in the western and north central parts and elevated temperatures in the eastern and northern parts of the study area, respectively.

Heat flow computed from 1 ó D modelling software and calibrated against BHT and reservoir temperatures suggests heat flow variations in the Niger Delta to range from 29 ó 55 mW/m² (0.69 ó 1.31 HFU) with an average value of 42.5 mW/m² (1.00 HFU). Lower heat flows ($< 40 \text{ mW/m}^2$) occur in the western and north central parts of the parts of the study area, and is likely to be influenced by high sedimentation rates. Higher heat flows (40 - 55 mW/m²) occur in the eastern and northwestern parts of the study area. Radiogenic heat production from crustal rocks and shaleøs may account for the heat flow in the east. Hydrothermal convection is likely to have elevated the heat flow in the northwest.

The hydrocarbon maturity modelling results show vast differences in timing and levels of kerogen transformation into petroleum. Result suggests that the potential source rocks (Paleocene, Eocene, Oligocene and partially the Lower Miocene) have attained maturity status to generate hydrocarbons. The depth to the onset of the oil window decreases from the west to the east and to the northwest.

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CHAPTER ONE

1.0 INTRODUCTION

1.1 General Introduction

A good knowledge of the geothermal gradients, subsurface temperature distribution and heat flow regime is invaluable in understanding the thermal maturation patterns of sediments as well as in unravelling the past thermal regimes in an area. The maturation of disseminated sedimentary organic matter into petroleum and its conversion to oil and natural gas is usually controlled by the temperature history of the sedimentary basin.

It is well established that the thermal history of a sedimentary basin is closely related to the mechanisms of basin formation (Sleep, 1971; McKenzie, 1978) and the development of suitable environments for the maturation of hydrocarbons. The implication for petroleum exploration is that the present day temperature field contributes to the probability of occurrence of economic hydrocarbon reserves. It is therefore appropriate to assess carefully the present thermal regime in the Niger Delta basin, where hydrocarbon exploration has been going on since the late 1950s. The database from which geothermal gradients, subsurface temperature and heat flow variations were estimated came from about seventy wells in the Niger Delta.

The Niger Delta is considered as one of the most prolific hydrocarbon provinces in the world, and recent oil discoveries in the deep-water areas suggest that the region will remain a focus of exploration activities for a long time to come (Corredor *et al*, 2005). In this study, the present day temperature data will serve as the basis for studying the thermal structure of the Niger Delta basin.

1.2 Location of the Study Area

The study area lies between longitudes $6^{\circ}30\,\text{gE} - 8^{\circ}00\,\text{gE}$ and latitudes $4^{\circ}00\,\text{gN} - 5^{\circ}00\,\text{gN}$. This is approximately between Easting 460,000.00-620,000.00 and Northing 8,000. - 112, 000.00 lying within the Eastern parts of the Niger Delta. The area spans about three depobelts: the Central Swamp, the Coastal Swamp and the Shallow Offshore depobelt of the Eastern Niger Delta of Nigeria. (Fig.1.1). The list of wells used for the study is shown in table 1.1.

1.3 Statement of the Problem

The Niger Delta sedimentary basin of Nigeria contains more than 12km of marine and deltaic sediments. Recent interests in drilling high-risk depths and targets such as the turbidite and channel fill facies of the Akata Formation, requires a good knowledge of the geothermal gradients and subsurface temperature variations. This study will therefore help in predicting temperatures prior to drilling, so that high temperature drilling bits, as well as well mud cementing programmes suitable for drilling such high-risk targets could be designed. This study will also be useful in basin analysis for evaluating the hydrocarbon maturation status. This work is therefore aimed at characterizing the thermal structure of the Niger Delta as well as illustrating its hydrocarbon maturation status. The processes responsible for the recognised thermal anomalies will also be highlighted.

Again conflicting views exists concerning possible source rocks in the Niger Delta. Some workers attribute the generated hydrocarbons as being sourced solely from Akata Formation with little or no contribution from the Agbada Formation (Evamy et al, 1978; Bustin, 1988 and Stacher, 1995), while others suggest variable

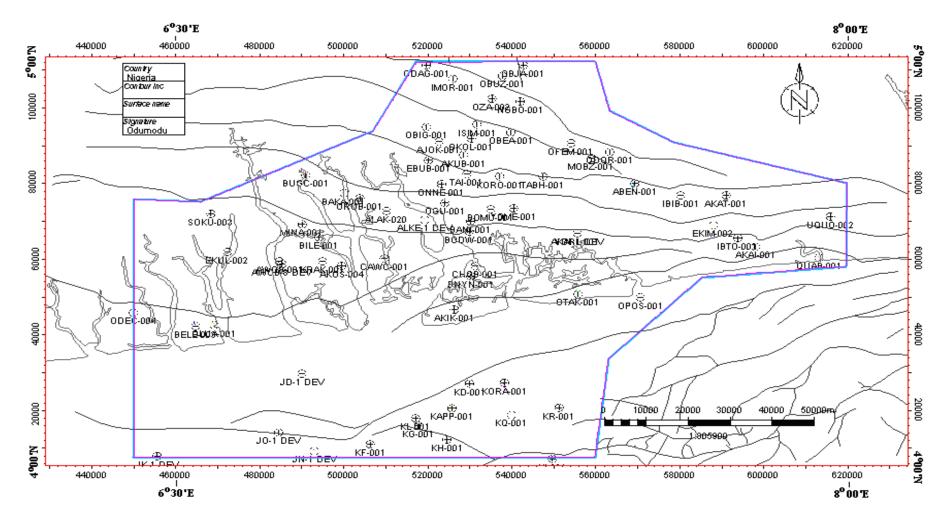


Figure 1.1: Map of the study area showing the three depobelts, wells used for the study and the the regional faults

| | TABLE 1.1: LIST OF WELLS USED IN THE STUDY | | | | |
|-----|--|-----|---------------|---------------|--|
| S/N | Well Names | OML | Class of well | Depobelts | |
| 1 | AKATA-001 | 13 | Е | Central Swamp | |
| 2 | ABAK ENIN-001 | 11 | Е | ,, | |
| | AKUBA-001 | 11 | E | ,, | |
| 4 | AJOKPORI-001 | 11 | E | " | |
| 5 | EBUBU-001 | 11 | E | " | |
| 6 | ISIMIRI-001 | 11 | E | ,, | |
| 7 | IMO RIVER-001 | 11 | D | ,, | |
| 8 | MOBAZI-001 | 11 | E | " | |
| | NGBOKO-001 | 11 | E | ,, | |
| 10 | KOROKORO-001 | 11 | А | ,, | |
| 11 | IBIBIO-001 | 13 | А | ,, | |
| 12 | OBEAKPU-001 | 11 | D | ,, | |
| | OBIGBO-001 | 11 | E | ,, | |
| | ODAGWA-001 | 11 | А | ,, | |
| | ODORO IKOT-001 | 11 | E | ,, | |
| | OFEMINI-001 | 11 | E | ,, | |
| 17 | OKOLOMA-001 | 11 | E | ,, | |
| 18 | ONNE-001 | 11 | E | ,, | |
| | OZA-002 | 11 | А | " | |
| 20 | TABANGH-001 | 11 | E | " | |
| 21 | TAI-001 | 11 | E | ,, | |
| 22 | AKAI-001 | 13 | E | ,, | |
| 23 | AKASO-004 | 18 | А | Coastal Swamp | |
| 24 | AKIKIGHA-001 | 11 | E | ,, | |
| 25 | ALAKIRI EAST-001 | 11 | E | ,, | |
| - | ALAKIRI-020 | 18 | A | ,, | |
| - | AWOBA-001 | 24 | E | ,, | |
| - | AWOBA-008 | 24 | E | ,, | |
| | BAKANA-001 | 18 | E | " | |
| | BANIELE-001 | 11 | E | " | |
| | BELEMA-003 | 25 | E | " | |
| | BILLE-001 | 18 | E | " | |
| _ | BODO WEST-001 | 11 | E | ,, | |
| | BOMU-001 | 11 | E | " | |
| _ | BONNY NORTH-001 | 11 | E | " | |
| | BUGUMA CREEK-001 | 18 | E | ,, | |
| | CAWTHORNE CHANNEL-1 | 18 | A | ,, | |
| - | CHOBIE-001 | 11 | E | ,, | |
| - | EKIM-002 | 13 | E | ,, | |
| | EKULAMA-002 | 24 | Α | ,, | |
| | IBOTIO-001 | 13 | E | ,, | |
| - | KRAKAMA-013 | | A | ,, | |
| | MINAMA-001 | 18 | E | ,, | |
| - | ODEAMA CREEK-004 | 29 | A | ,, | |
| 45 | OGU-001 | 11 | E | ** | |

| | TABLE 1.1: LIST OF WELLS USED IN THE STUDY | | | | | |
|--------|--|-----|---------------|------------------|--|--|
| S/N | Well Names | OML | Class of well | Coastal Swamp | | |
| 46 OF | POBO SOUTH-004 | 11 | А | 33 | | |
| 47 OF | RUBIRI-001 | 18 | E | ,, | | |
| 48 OT | TAKIKPO-001 | 11 | E | ,, | | |
| 49 OL | _UA-001 | 25 | Е | ,, | | |
| 50 QL | JA IBO-001 | 13 | Е | ,, | | |
| 51 SC | DKU-003 | 23 | Ш | 33 | | |
| 52 UC | QUO-002 | 13 | Ш | 33 | | |
| 53 YC | DMENE-001 | 11 | Е | ,, | | |
| 54 YC | ORLA-001 | 11 | E | 33 | | |
| 55 KC | DRONAMA-001 | 72 | Е | Shallow Offshore | | |
| 56 KA | APPA-001 | 72 | Ш | 33 | | |
| 57 KR | २-001 | 72 | Е | ,, | | |
| 58 KF | F-001 | 72 | Е | ,, | | |
| 59 KG | G-001 | 72 | Е | 33 | | |
| 60 KH | H-001 | 72 | Е | ,, | | |
| 61 KD | D-1 | 72 | Ш | 33 | | |
| 62 KI- | -001 | 71 | Ш | 33 | | |
| 63 KG | Q-001 | 72 | Е | ,, | | |
| 64 KL | 001 | 72 | Е | 33 | | |
| 65 JA | A-001 | 74 | Е | 3 7 | | |
| 66 JD | 0-001 | 74 | Е | ,, | | |
| 67 JK | K-001 | 74 | E | ,, | | |
| 68 JK | 6-002 | 74 | E | 3 3 | | |
| 69 JN | J-001 | 74 | E | 33 | | |
| 70 JO | D-001 | 74 | E | ,, | | |

contributions from both formations (Lambert-Aikhionbare and Ibe, 1984) and even from deeper sources (Haack et al, 1997; Stephens et al, 1997)

This work therefore evaluates the hydrocarbon maturation status of Miocene to Paleocene source rocks using the burial and thermal history of the basin.

1.4 Scope of Previous Studies

The Niger delta sedimentary basin of Nigeria has been a focus of so many geological studies because of the petroleum potentials of the area. Most of these studies range from sedimentological / stratigraphic, biostratigraphic, paleontological, geophysical to petroleum geology. However few geothermal studies that have been done in Niger Delta include the works of Nwachukwu (1976), Avbovbo (1978), Evamy *et al* (1978), Chukwueke *et al* (1992), Brooks *et al* (1999), Akpabio *et al* (2003) and Ogagarue (2007). Subsurface temperatures variations and heat flow in the adjacent Anambra basin has also been studied by Onuoha and Ekine (1999).

Nwachukwu (1976) examined about 1000 well logs from the Niger Delta basin and discovered that the geothermal gradients are lowest over the centre of the Niger Delta, approximately about 0.7 to 1.0°F/100ft, and increase to about 3°F/100ft in the Cretaceous rocks on the north. Evamy *et al* (1978), in his study on the hydrocarbon habitat of the Tertiary Niger Delta, investigated the relationship between sand percentage, depth and temperature. In that study, they showed that geothermal gradient increases with diminishing sand percentage from less than 1.0°F/100ft (1.84°C/100m) in the continental sands to about 1.5 °F/100ft (2.73 °C/100m) in the paralic section, to a maximum of about 3.0°F/100ft (5.47°C/100m) in the continuous shales of the Niger Delta. Avbovbo (1978) utilized electric logs (Bottom Hole Temperatures) and production reservoir temperatures data from southern Nigeria

basin to determine geothermal gradients in the Niger Delta. His geothermal gradient map based on one hundred and sixty temperature depth plots showed an increase in temperature gradient to the North-east, with the highest gradient of 3.00° F/100ft occurring in the Awgu-Enugu-Nsukka axis of the Anambra Basin, fairly high temperature gradients of about 1.60 to 2.60° F/100ft in the Calabar-Onitsha óBenin axis of the Coastal region and low gradients of about 1.20 to 1.40° F/100ft in the Warri-Port-Harcourt areas of the Niger Delta, while in the offshore areas the maximum temperature gradient is about 1.80° F/100ft. He also showed that geothermal gradients are quite higher at the flanks. The maximum temperature gradient at the northeastern flank is about 2.60° F/100ft and 2.20° F/100ft at the eastern flank. Chukwueke *et al* (1992) in their study of the sedimentary processes, eustatism, subsidence and heat flow in the distal part of the Niger Delta, has shown that geothermal gradients determined from 33 wells range between 19 - 32° C / km while heat flow varies from 45 - 85 mWm⁻².

Brooks *et al* (1999), conducted regional heat flow measurements at 112 sites on the continental margin, offshore Nigeria, for the primary purpose of determining basal heat flow for thermal maturation studies of the petroleum systems. The result of their study shows that heat flow in the area ranged between 18.8 - 123.7 mWm⁻², with an average of 58.2 mWm⁻², and a predominance of heat flow between 40 and 70 mWm⁻². Ogagurue (2007) determined heat flow estimates from twenty-one wells in the western Niger Delta Basin. The heat flow estimates vary between 27.6 mWm⁻² -68.3 mWm⁻², with a simple average of 43.92 mWm⁻². He concluded that the northcentral part of the study area is characterized by high heat flow, which decreases towards the Niger Delta coast. Akpabio *et al* (2003) determined geothermal gradients in the Niger Delta using continuous temperature logs from 260 wells and discovered that geothermal gradients in the continental section are lowest ($0.82^{\circ}C/100m$) in the central part of the delta, increases seaward to $2.62^{\circ}C/100m$, and northward to $2.95^{\circ}C/100m$. Also in the marine/paralic section, the geothermal gradients range from $1.83^{\circ}C/100m$ to $3.0^{\circ}C/100m$ at the central parts of the delta, to between $3.5^{\circ}C/100m$ and $4.6^{\circ}C/100m$ northwards and $2.0^{\circ}C/100m$ and $2.5^{\circ}C/100m$ seawards. Onuoha and Ekine (1999) studied subsurface temperature variations and heat flow in the adjacent Anambra Basin and calculated geothermal gradients and heat flow estimates that varies between $25 - 49 \pm 1^{\circ}C/km$, and $48 - 76 \pm 3mWm^{-2}$ respectively.

1.5 Purpose and Scope of Present Research

The aim of this research is to study subsurface temperature distributions, geothermal gradients, thermal conductivity, heat flow variations, burial history and hydrocarbon maturation modelling in the Central Swamp, Coastal Swamp and Shallow Offshore depobelts of the Eastern Niger Delta.

The technical objectives set for this study include;

- i. To produce temperature / depth profiles of some of the wells in the two depobelts
- ii. To estimate the geothermal gradients in the various depobelts
- iii. To produce reliable subsurface temperature distribution maps and geothermal gradient maps.
- v. To estimate the heat flow variations in the depobelts
- vii To assess the burial history and hydrocarbon maturation
- iv. To assess the timing and depth of hydrocarbon generation

Seventy wells, which include exploration, appraisal, and development wells, owned by the Shell Petroleum Development Company of Nigeria Limited were used for this study (Table 1.1)

In this study, subsurface temperatures and geothermal gradients were evaluated using production reservoir temperature logs supplemented by corrected bottom hole temperature data. The choice of reservoir temperature data is predicted on the fact that they are generally considered alongside with continuous temperature logs as being closer to formation equilibrium temperatures. The continuous temperature logs were not used because they are available only for very few fields such as Bomu, Ekulama and Opobo South, within the study area.

The temperature and burial history of a sedimentary basin is crucial in accurately evaluating its hydrocarbon maturation status. This study is therefore necessary so that it can provide some qualitative and quantitative information on the thermal status of these three depobelts in the eastern part of the Niger Delta. In this study the factors influencing the variations in geothermal gradients, temperature distribution patterns and certain geological and structural features of these parts of the delta will be highlighted.

This study is also significant in the sense that this study will facilitate the exploration studies in this part of the delta and also in the deep play prospects of the offshore Niger Delta. It has been noted that the deeper, over pressured shales of Akata Formation have not been drilled. Drilling in such areas requires an accurate assessment of the hazard risks associated with drilling in high-pressure, high-temperature conditions. This study will also be necessary for designing well mud and cementing programmes for drilling in such a high-risk area.

CHAPTER TWO

2.0 GEOLOGIC AND STRUCTURAL SETTING

2.1 Background Geological Information of

2.1.1 Lithostratigraphy the Niger Delta

The Tertiary Niger Delta covers an area of approximately 75,000 sq km and consists of a regressive clastic succession, which attains a maximum thickness of 12,000m (Orife and Avbovbo, 1982). The Niger delta is located in the Gulf of Guinea, Central West Africa, at the culmination of the Benue Trough (Figure 2.1) and is considered one of the most prolific hydrocarbon provinces in the world (Corredor et al, 2005). The Anambra basin and Abakaliki High to the north, the Cameroun volcanic line to the east, the Dahomey Embayment to the west and the Gulf of Guinea to the south define the boundaries of the Niger Delta. Burke (1972) remarked that the siliciclastic system of the Niger Delta began to prograde across pre-existing continental slope into the deep-sea during the Late Eocene and is still active today. The lithostratigraphy of the Tertiary Niger Delta (Figure 2.2 and 2.3) can be divided into three major units: Akata, Agbada and Benin formations, with depositional environments ranging from marine, transitional and continental settings respectively. The Akata, Agbada and Benin formations overlie stretched continental and oceanic crusts (Heinio and Davies, 2006). Their ages range from Eocene to Recent, but they transgress time boundaries. These prograding depositional facies can be distinguished mainly on the basis of their sand-shale ratios.

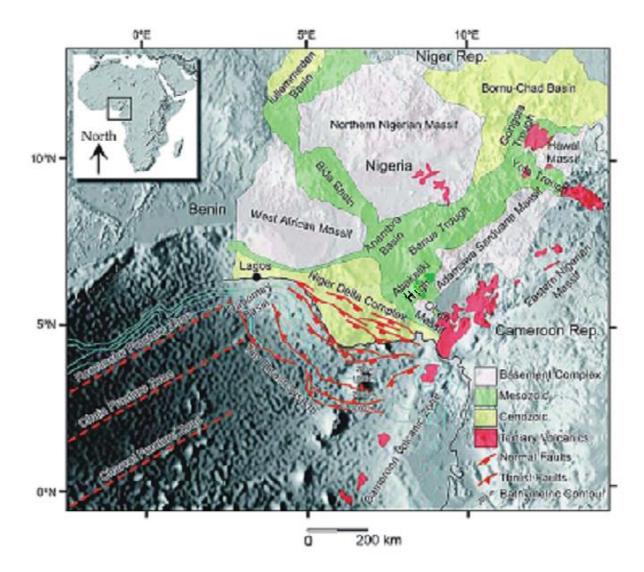


Figure 2.1: Map of Nigeria showing the Niger Delta Complex, the Anambra Basin & the Benue Trough (After Corredor et al, 2005)

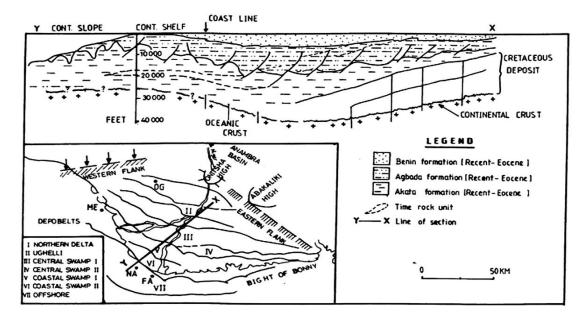


Fig 2.2: Niger Delta: Stratigraphy and Depobelts (Ekweozor and Daukoru, 1984)

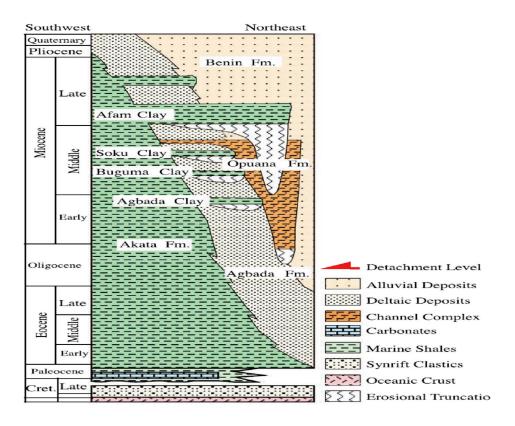


Fig. 2.3: Regional Stratigraphy of the Niger Delta (Lawrence et al, 2002; Corredor et al,

2005

2.1.1.1 The Akata Formation

The Akata Formation is the basal sedimentary unit of the delta. It consists of uniform dark grey over-pressured marine shales with sandy turbidites and channel fills. Its age ranges from Late Eocene to Recent. In deep-water environments, these turbidites are the potential reservoirs. Whiteman (1982) suggested that the Akata Formation may be about 6,500m (21,400 ft) thick, while Doust and Omatsola (1990) suggested that the thickness ranges from 2000 m (6600 ft) at the most distal part of the delta to 7000 m (23,000 ft) beneath the continental shelf. Corredor *et al* (2005) also suggested a thickness of about 5000m (16,400 ft) for the deep fold and thrust belts in the offshore Niger Delta. The Akata Formation has generally been regarded as the main source rock for oil in the delta.

2.1.1.2 The Agbada Formation

This is the major petroleum-bearing unit in the Niger Delta. It overlies the Akata Formation and consists of alternations of sand and shale layers. The Agbada Formation is characterized by paralic to marine-coastal and fluvial-marine deposits mainly composed of sandstone and shale organized into coarsening upward off-lap cycles (Pochat *et al*, 2004). According to Corredor *et al* (2005), the Agbada Formation consists of paralic siliciclastics that are more than 3500 m (11,500 ft) thick and they represent the actual deltaic portion of the succession that accumulated in delta front, delta-top set and fluvio-deltaic environments. The first occurrences of shale with marine fauna usually characterizes the top of the Agbada Formation while the deepest significant sandstone body characterizes the base. The Agbada Formation can be subdivided into upper, middle and lower units. The upper unit is made up of 60 - 40 percent sand. The middle unit consists of 50 6 30 percent sand and is the main

objective of oil and gas exploration in the delta. The lower unit is made up of 20 percent sand inter-bedded with under-compacted shales.

2.1.1.3 The Benin Formation

Onshore and in some coastal regions, the Benin Formation overlies the Agbada Formation. The Benin Formation consists of Late Eocene to Recent deposits of alluvial and upper coastal plain deposits that are up to 2000 m (6600 ft) thick (Avbovbo, 1978).

2.1.2 Depositional Belts

Depositional belts or õdepobeltsö consists of a series of off-lapping siliciclastic sedimentation cycles or mega-sedimentary belts. Evamy *et al* (1978) referred to this structure as, õmega structureö while Doust and Omatsola (1990) were the first to call them õdepobeltsö. Five regional depobelts can be discerned along the north ó south axis of the delta, each with its own sedimentation, deformation and petroleum history. These depobelts include: the Northern Delta, the Greater Ughelli, the Central Swamp I & II, the Coastal Swamp and the Offshore depobelts (Figure 2.2). Each of these depobelts is bounded by large-scale regional and counter-regional growth faults (Evamy *et al*, 1978; Doust and Omatsola, 1990; Pochat *et al*, 2004). The activity in each belt has progressed in time and space toward the south-southwest through stepwise alluvial progradation facilitated by large-scale withdrawal and forward movement of the underlying shale. The interplay of subsidence and supply rates resulted in deposition of discrete depobelts ó when further crustal subsidence of the basin could no longer be accommodated, the focus of sediment deposition shifted seaward, forming a new depobelt (Doust and Omatsola, 1990).

2.2 Regional Structural Setting

The Niger Delta remains the best-studied part of Nigeriaøs continental margin because of its rich hydrocarbon resources. An averaged section of the Niger Delta as drawn by Thomas (1999) is shown in figure 2.4, illustrating the diapiric structures on the continental slope and rise as well as the faulting of the Oligocene and younger formations.

In the Niger Delta, the continental shelf is about 50 to 80 km in width and the shelf break occurs at depths between 150 to 200 m (Fig 2.5). The continental slope, which is steeper, extends from the shelf break to a distance of 2-3 km, where the more gently sloping continental rise starts. The continental rise continues downslope to the abyssal plains of the Gulf of Guinea with water depths greater than 4.5 km. In the continental margin, from the outer shelf (shallow water) to the deep slope (deep water) of the Niger Delta, three distinct structural domains (Figure 2.5) have been observed from previous studies. These structural zones are:

- (I) an upper extensional domain dominated by growth faults beneath the continental shelf and upper slope;
- (II) a translational domain or an intermediate zone characterized by mud diapirism, and

(III) a lower compressional domain characterized by imbricate toe of slope thrusts.

According to Cohen and McClay (1996) as well as Morgan (2004), this structural configuration is caused by gravitationally driven delta tectonics, where the Agbada Formation is collapsing on a detachment in the Akata Formation.

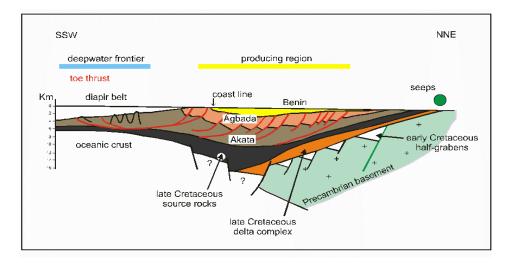


Fig. 2.4: Averaged section of the Niger Delta (After, Thomas, 1995,

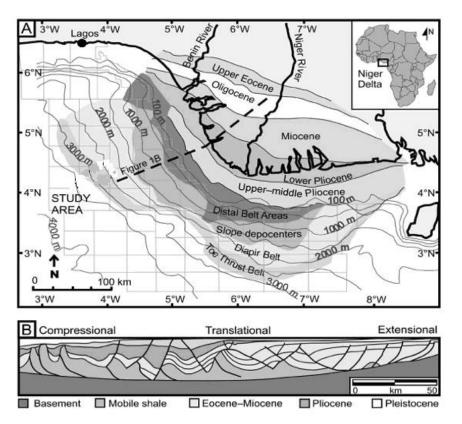


Fig. 2.5; Structural domains of the continental shelf, slope and rise of the offshore Niger Delta (After Cohen and McClay, 1996

2.2.1 Structural Evolution of the Niger Delta

Several workers including Burke *et al* (1971), Whiteman (1982) and Olade (1975) has summarized the structural and tectonic setting of the Niger Delta. According to these authors, the structural evolution of the Niger Delta began with the formation of the Benue trough in the Early Cretaceous as a failed arm of a triple rift junction associated with the opening of the South Atlantic. Olade (1975) contends that the initial stage of the evolution involves the rise of a mantle plume in the region of the present Niger Delta, which led to the doming and rifting in the Benue region, developing an RRR triple junction. Three major tectonic phases or epirogenic movements were suggested by Murat (1972) to have influenced the geologic history of the Benue Trough system, which he subdivided into three paleogeographic areas or sub-basins; the AbakalikióBenue Trough, the Anambra Basin and the Niger Delta basin.

The initial rifting resulted to rapid subsidence and deposition of the Asu River Group during the Albian times. During the Cenomanian, a mild deformational event led to the compressive folding of the Asu River Group and restriction of the Odukpani Formation to the Calabar flank. Continued mantle upwelling and rifting during the Early Turonian resulted to the deposition of the Ezeaku Formation. When mantle upwelling finally ceased and migrated westward by the Santonian, the trough collapsed.

The second tectonic phase started during the Santonian as a gentle widespread compressive folding, uplifting the Abakiliki-Benue Trough. The Anambra Basin and the Afikpo Syncline subsequently subsided and were filled by two deltaic sedimentary cycles through to Palaeocene. The last tectonic phase resulted from the uplift of the Benin and Calabar flanks during the Paleocene ó Early Eocene (Murat, 1972). These movements initiated the subsidence and progressive outbuilding of the Eocene ó Holocene sediments of the Niger Delta along the Northeast-Southwest fault trend of the Benue Trough.

The structural evolution of the Niger Delta has been controlled by basement tectonics as related to crustal divergence and translation during the Late Jurassic to Cretaceous continental rifting. It has also been influenced by isostatic response of the crust to sediment loading. The Niger Delta has been rapidly subsiding because of sediment accumulation, flexural loading, and thermal contraction of the lithosphere (Onuoha, 1982, 1986; Onuoha and Ofoegbu, 1988). According to Caillet and Batiot (2003), throughout the geological history of the delta, its structure and stratigraphy have been controlled by the interplay between rates of sediment supply and subsidence. Subsidence itself has been controlled both by driving subsidence of the basement as well as differential sediment loading and compaction of unstable shales.

2.2.2 Structural Patterns of the Niger Delta

Evamy *et al* (1978) described the fault typeøs common in the Niger Delta. These faults include (a) structure building faults, (b) crestal faults (c) flank faults (d) counter regional growth faults as well as antithetic faults (Figure 2.6.) The structure building faults define the up-dip limit of major rollover structures. They are essentially concave in the down-dip direction and repeat each other en echelon. They also define the boundaries of depobelts or megastructures. The counter regional faults as their name implies are those faults that possesses a counter regional hade, including as well the antithetic faults. Large counter regional faults define the southern limits of depobelts. Crestal faults also occur within rollover structures. and are generally steeper in the vertical direction. They display less growth, which also tends to be less continuous. The flank structures occur at the southern flanks of major structures and show some major rollover deformation at shallow levels. These faults show southerly dips at depth. K-type faults are mainly flank faults, which are very closely spaced resulting to a multiplicity of narrow fault blocks. The K faults are very common in SPDC¢s offshore K- field.

The occurrence of synsedimentary faults, which deforms the delta beneath the Benin Formation, presents a very striking structural feature in the Niger Delta (Fig. 2.7). These synsedimentary faults are also known as growth faults while the anticlines associated with them are known as rollover anticlines. According to Whiteman (1982), they are called growth faults because they are frequently initiated around local depocentres and grow during sedimentation, thereby allowing a greater amount of sediment to accumulate in the down thrown block compared to the up thrown block. Caillet and Batiot (2003) suggested that growth faults were triggered by the movement of the deep-seated, over pressured, ductile marine shales and aided by slope instability.

Whiteman (1982) also defined a growth fault as a fault that offsets an active surface of deposition. Most growth faults in the Niger Delta are frequently crescent in shape with the concave side facing the down thrown side usually seawards. Most growth faults show a marked flattening with depth. They can be described as being listric in shape. These growth faults affect the Agbada and the Akata formations, and dies out below the base of the Benin Formation. These growth faults exhibit throws of several thousands of feet at the top of the Akata Formation whereas they die out to nothing at the base of the Benin Formation. In depth, growth faults may become thrusts and displacement may exceed many thousand feets in toe thrust zones. As noted by Doust and Omatsola (1990), the magnitude of throws on growth faults bounding depobelts is such that much of the paralic succession on the downthrown side is younger than that on the up thrown side. Within depobelts, growth faults form boundaries of macrostructures, each characterized by its own sand-shale distribution pattern and structural style.

Growth faults present a migratory path for hydrocarbons generated in the Akata and Agbada formations, thereby enabling them to migrate and accumulate in the reservoir sands within the Agbada Formation. The growth faults also act as seals to migration. When the throw of the fault exceeds the sand thickness, the fault zone serves as a seal but this depends on the amount of shale smeared into the fault plane.

Rollover anticlines always occur in association with the growth faults and it is in these structures that oil and gas in the Agbada reservoir sands have been noted.

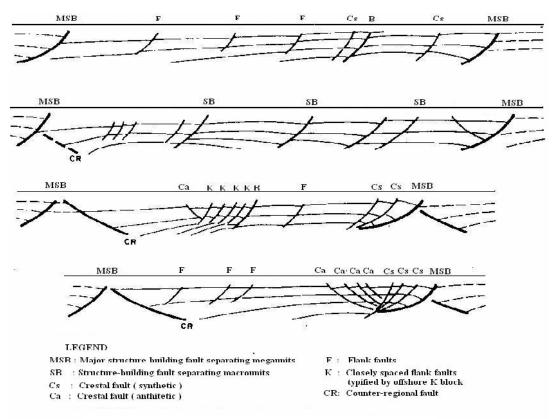


Fig. 2.6 : Megaunits and associated sedimentary fault types (Evamy et al, 1978)

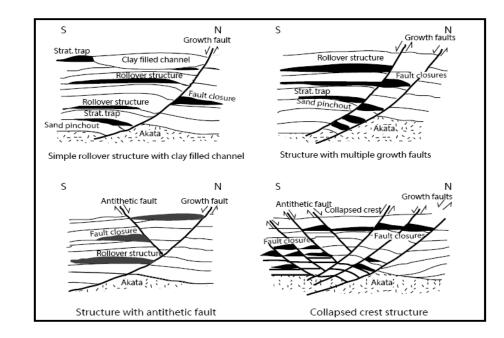


Fig. 2.7: Examples of Niger Delta field structures and associated traps (Doust and Omatsola, 1990, Turtle et al, 1999)

2.3 Source Rocks of the Niger Delta

The source rocks responsible for the hydrocarbon accumulation in the Niger Delta has been widely discussed in literature (e.g. Weber and Daukoru, 1975; Frost, 1977; Evamy *et al.*, 1978; Ejedawe *et al*, 1979; Ekweozor *et al*, 1979; Ekweozor and Okoye, 1980; Ekweozor and Daukoru, 1984; Lambert Aikhionbare and Ibe, 1984; Bustin, 1988; Doust and Omatsola, 1990; Stacher, 1995; Haack *et al*, 1997). Some of these authors attributed the generated petroleum solely to the source rocks of the Akata Formation, while others suggests variable contributions from the marine interbedded shales in the lower Agbada Formation and the marine Akata Shale and possibly a Cretaceous source.

These controversies as to the possible source rocks in the Niger Delta were generated by the known poor source rock qualities of the Agbada Formation and the Akata Shale. According to Lambert-Aikhionbare and Ibe (1984), the Agbada shales contain moderate total organic carbon and type II to II-III kerogen. These source rocks give low rock eval pyrolysis yields (i.e. hydrogen index < 200mgHC/g organic carbon) and vitrinitic, gas prone kerogens (Nwachukwu and Chukwura, 1986; Bustin, 1988). Evamy *et al* (1978) and Stacher (1995) suggested that the Agbada Formation does not have the sufficient thickness and maturity to be a potential source rock.

The Akata shales have been poorly sampled because of their great depths and also due to the undercompacted and overpressured sediments. The source rocks contain a lot of terrigenous organic matter even though they were deposited in a more open marine than a deltaic environment (Bustin, 1988). The paucity of known good to excellent oil-prone source rocks is responsible for the petroleum occurrence in the delta being attributed to the large volume of source rocks rather than to the organic richness (Bustin, 1988). A recent study by Haack *et al* (1997) suggests a correlation between oils and source rock in the Early Tertiary. In this work, the Upper Cretaceous ó Lower Palaeocene and Upper Eocene are suggested as potential source rocks. Stephens et al (1997) found a source potential in the Oligocene in the southeastern Niger Delta, offshore Equatorial Guinea.

2.4 Hydrocarbon Properties of the Niger Delta

The physical and chemical properties of the Niger Delta crude oils are highly variable, even to the reservoir scale. According to Whiteman (1982), the oil within the delta has an API gravity range of 16 \circ 50 $^{\circ}$ API, with the lighter oils having greenish colours. It is also noted that about fifty-six percent of the oils in the delta have API gravity between 30° and 40°.

Evamy *et al* (1978) classified Niger Delta crude oil into light and medium gravity crudes. The light crudes are characteristically paraffinic and waxy, with pour points from 67 to 32 $^{\circ}$ C (20 to 90 $^{\circ}$ F). Their wax contents are about 20%, but commonly around 5 %. They occur in the deeper reservoirs. The medium crudes are dominantly naphthenic, non-waxy, with pour points less than 625 $^{\circ}$ C (-13 $^{\circ}$ F). The medium gravity crudes has a specific gravity that is greater than 0.90 (< 26 $^{\circ}$ API).

Evamy *et al* (1978) also noted that the distribution of crudeøs according to their tank-oil specific gravity and pour point shows the heavy, low pour point crudes to be consistently above the lighter, high pour-point varieties. The quality of crude oil in the Niger Delta has also been shown to be more dependent on temperature rather than depth. Evamy *et al* (1978) has shown that the heavy naphthenic oils are paraffinic oil that have undergone bacterial transformation or biodegradation in the shallow cooler reservoirs and belong to the same family as the paraffinic waxy oils that occur in deeper high temperature reservoirs. Based on the fact that biodegraded oils occur only in shallow traps within the temperature regime that bacteria can survive, they suggested that a late migration within no noticeable subsidence of the trap after its emplacement. Matava *et al* (2003) also showed that compositional variations in Niger delta crudes results from migration rather than source rock organic matter input or thermal maturity.

The concentration of sulphur in the Niger Delta crude oil is low, between 0.1% and 0.3%, with a few samples having concentrations as 0.6% (Nwachukwu *et al*, 1995).

CHAPTER THREE

3.0 BACKGROUND ON THERMAL STUDIES

3.1 Thermal Studies

Geothermal studies is useful in understanding many of the geological and geophysical phenomena that is being witnessed on the earth, such as earthquakes and volcanism as well as the earth¢s magnetic field and the plasticity of earth¢s material at depth. Heat flow studies also give us insight into the thermal history and geodynamic origin of sedimentary basins. According to Jessop and Majorowicz (1994), the thermal history of a basin depends on its tectonic origin and the circumstances of its development. The dissipation of excess heat associated with basin formation and the transfer of the continuous heat supply from the basement depend on the thermal properties of the strata and their water content. The thermal conditions of a sedimentary basin is usually influenced by the heat flow from the underlying basement and the thermal conductivity of the sedimentary cover or overprinted by other processes such as fluid flow (Forster, 2001)

Present-day temperature data is most often used in studying the thermal structure of the earth. The thermal gradient and thermal conductivity values of rock types in an area have been used to obtain estimates of heat flow variations in an area. The variations in heat flow in a sedimentary basin are influenced by several factors, which include:

| Ι | Basement Heat flow |
|-----|--|
| II | Radioactive Heat Production in sediments |
| III | Effect of Sedimentation |
| IV | Deeply buried salt structures |
| V | Fluid flow through sediment |

I. Basement Heat Flow

Basement heat flow is primarily controlled by the mechanics of the basinforming rift-extension event and subsequent subsidence caused by the cooling of the lithosphere (McKenzie, 1978; Sclater and Cerlerier, 1987). Heat flow decreases with time as the lithosphere gradually approaches a quasi-steady state (Sclater and Christie., 1980). Beardsmore and Cull, (2001) observed that the heat generated through the radioactive decay of unstable elements, such as uranium, thorium and potassium contained in the crustal rocks has a significant contribution to the total heat flow coming from the basement. The continental crust is also known to produce several tens of time more radiogenic heat than the oceanic crust.

II Radiogenic Heat Production in Sediments

Clastic sediments such as shale contain quite a lot of radiogenic heatproducing elements such as thorium, uranium and potassium. The sediments contribute its radiogenic heat to the total heat flux travelling up in the column. The contribution of radiogenic heat to seafloor heat flow is proportional to the total thickness of the sediments.

III Effects of Sedimentation

Sedimentation influences surface (Seafloor) heat flow (Hutchison, 1985; Wang and Davies, 1992). All agree on an inverse relationship between sedimentation and sea floor heat flow (i.e. faster sedimentation rate, lower heat flow and vice versa). IV Deeply buried Salt structures

Two factors commonly control salt-induced heat flow anomalies (OøBrien and Lerche, 1984; Corrigan and Sweat, 1995). These factors are: the depth of burial and the thickness or height of the salt body relative to its width. A tall piercing diapiric plug would cause a large heat flow anomaly whereas a laterally extensive, bedded salt body would not show any anomaly. Nagihara *et al* (1992) observed that diapiric induced heat flow anomalies are localized directly above the salt body.

V Fluid flow through sediments

The sedimentary thermal regimes can be perturbed by the vertical migration of pore fluids and seeps on the sea floor. Anderson *et al* (1991) observed that heat flow measurements made close to the upward migration path of the seeps shows that the values are higher than those beside it.

3.2 Heat Transfer Mechanisms

Three basic ways exist through which heat can be transferred through rocks. These include convection, conduction and advection. Convection involves heat transfer by which the motion of the fluid carries heat from one place to another. Convection currents are set up in the fluid because the hotter part of the fluid is not as dense as the cooler part, so there is an upward buoyant force on the hotter fluid, making it rise while the cooler denser fluid sinks. In conduction, the substance itself does not flow; rather vibrations transfer heat energy internally, from atom to atom within a substance. Conduction is most effective in solids. Advection involves convective energy transfer through fault planes.

In the Akata and Agbada formations, the predominant heat transfer mechanisms are conduction and advection through some major faults. Because of fresh water circulation, the predominant heat transfer mechanism in the Benin Formation is convection.

3.3 Determination of Static Formation or Virgin Rock Temperatures

The temperature logs used in determining static (equilibrium) formation temperatures include (i) Bottom hole temperature logs (ii) Continuous temperature logs and (iii) Production Reservoir temperature logs.

The Continuous Temperature logs and the Production Reservoir temperature logs have been considered in a lot of studies as being close to the static formation temperature. Forster (2001) observed that continuous temperature logs reflect true formation temperatures because of the fact that the time prior to the logging was enough for the borehole to regain thermal equilibrium after the drilling process.

Bottom-hole temperatures are routinely recorded during wire-line logging operations and thus are usually the commonest type of subsurface temperature measurements available from hydrocarbon exploration activities. Nagihara and Smith (2005) described the method from which bottom-hole temperatures were obtained. According to them, bottom hole temperature measurement is obtained shortly after the well has been shut in. After drill fluid circulation ceases, a string of logging tools, which includes a temperature censor, is lowered. When the tool string returns to the surface, the maximum-recorded temperature is reported in the log header, along with the time the well is shut in and the time the tool string reached the bottom. BHT measurements can be made at several depths in a well while the well is deepened during drilling. It has been noted in several studies that bottom-hole temperature values are considerably lower than the true formation temperature, or virgin rock temperature, because of the cooling effect of the drill-fluid circulation (Forster, 2001; Nagihara and Smith, 2005 & 2008; Cory and Brown, 1998; Chulli et al, 2005). Nagihara and Smith (2008) reported that temperature difference between bottom-hole temperature and virgin rock temperature as being dependant on many factors involved in the fluid circulation such as borehole size, depth of the formation, formation thermal properties, and the timing of the bottom hole temperature measurement relative to the shutting in of the well. If the borehole is left undisturbed for sometime after drilling, the temperature inside and around it will gradually recover to its pre-drilling state. This recovery can take weeks or months and so it is not logistically possible to keep the well shut for a full recovery. So multiple BHT measurements for a short period of time (1-2 days) at a particular depth can reveal the temperature recovery trend which can be theoretically extrapolated to determine the equilibrium temperature.

There are several methods for estimating static formation temperatures from bottom-hole temperatures. These include: (I), using the Hornerøs plot method of Bullard (1947) and (ii) correcting BHT data based on CTL (Continuous temperature logs) and PRT (Production reservoir) temperature logs as references for correction.

The Hornerøs method has been the most widely used technique and requires two or more BHT measurements at different times and at the same depth to monitor the return to equilibrium temperature after drilling has ceased (Cory and Brown, 1998). According Nagihara and Smith (2005), the BHT measurements obtained at different times should show the well bore temperature slowly recovering towards its pre-drilling state. The Hornerøs plot method is given by the following equation:

$$T_{equil} = T_{BHT} - M \operatorname{In} \begin{bmatrix} t_{shut - in} + t_{circ} \\ t_{shut - in} \end{bmatrix} - \dots - (1)$$

Where T_{equil} represents the equilibrium temperature (°C), T_{BHT} represents

the bottom hole temperature (°C), $t_{shut-in}$ represents the shut in time, t_{circ} represents the circulation time and M represent the Horner slope. A Horner slope is produced by plotting T_{BHT} values against the corresponding $In[(t_{shut-in} + t_{circ})/t_{shut-in}]$ values for a particular run. The slope M and intercept T_{equil} can be determined using linear regression. Therefore for each run in a well where two or more BHTs are measured at the same depth but at different shut-in times, a Horner plot can be used to estimate the equilibrium temperature.

According to Cory and Brown (1998) some quality control that must be applied to BHT data before it is used in estimating equilibrium or static formation temperature include that: (1) Each sequence of BHT measurements recorded at the same depth during a logging run generally shows a smooth increase in temperature as the shut-in time increases. Any BHT, which showed an irregular increase or decrease, thereby disrupting the pattern should be removed from the dataset. (2) The accuracy of the Horner plot should increase with the increasing shut-in time. BHTs measured after a short shut-in time period are unsuitable for the Horner plot method. BHTs measured with a shut-in time < 2 hours should be removed. (3) The circulation time is not a sensitive parameter in the Horner plot method (Luheshi, 1983; Brigaud *et al*, 1992) A circulation time of 2 hours is mostly been assumed in some studies.

Chapman *et al* (1984) utilized the Horner plot method to correct bottom hole temperatures data to static formation temperatures in the Uinta basin. The relation is given as:

$$T_{B(t)} = T_{B(\alpha)} + A \log \left(\frac{t_c + t_e}{t_e}\right)$$
(2)

The ordinate intercept on the semi-log plot of $(t_c + t_e)/t_e$ versus T, gives the estimate of $T_{B(\alpha)}$, which is the equilibrium or static formation temperature.

Leblanc *et al* (1981) suggested a method of correcting bottom hole temperatures based on Middleton (1979) curve matching technique whereby thermal stabilization curves derived from an assumed thermal diffusivity are superimposed on actual data to estimate a true formation temperature. Leblancøs relation is given as:

BHT
$$(0, t) = T_m + \Delta T \left[e^{-a^2} / 4_{Kt} \right]$$
....(3)
Where $\Delta T = T_f - T_m$

 T_m = the temperature of the drilling mud before circulation

 T_f = the formation temperature

a = the drill hole radius

K = the formation rock diffusivity constant

t = the total time of mud circulation at the depth of measurement,

and T_f = the formation temperature

Luheshi (1983) proposed a relation for determination of formation temperature T_f from bottom hole temperature $T_{(a,t)}$, which is space and time dependent. Luheshis relation is given as:

Where $t_2 = t - t_1$, is the shut in time after the end of mud circulation?

t, is the duration of drilling and, t_1 the total mud circulation time at the depth of measurement. K, is the diffusivity of the formation rock type, a is the borehole radius while $T_{(a,t)}$ i.e. Q is the heat flow at the depth of measurement.

The above relation is valid when $T_{(a,t)}$ measured at depth is more than ten times borehole radius above the bottom of the well and $a^2/4kt_2$ is less than unity.

Shen and Beck (1986) utilized laplace transforms to derive analytical models for BHT stabilization, in which drilling mud circulation effects, thermal property contrast between the formation and the borehole mud and presence of radial or lateral fluid flow are considered.

The other method is based on a statistical approach that uses continuous temperature logs (CTL) and Production reservoir temperatures (PRT) as references for correcting bottom-hole temperatures.

3.4 Geothermal Gradients and Heat Flow Determinations

There are two basic approaches in calculating thermal gradients. These include the thermal resistance or Bullardøs method and the simple gradient method (Chapman *et al*, 1984).

Thermal resistance is defined as the quotient of the thickness Δz and a characteristic thermal conductivity k and is given by the equation

$$T_B = T_o + q_o \sum_{z=0}^n \left(\frac{\Delta z}{k}\right) \tag{5}$$

Where (T_B) is the temperature at depth z = B, T_0 , the surface temperature at z = 0

 q_{o} , the surface heat flow and $\left(\frac{\Delta z}{k}\right)$, the thermal resistance, which is summed for all rock units from the surface to the depth B.

Heat flow (q_o) can be calculated as the slope of the plot of the consecutive values of T_B versus the summed thermal resistance (R_i) to the measurement depth.

The steps required in using this method to estimate heat flow and subsurface temperatures in a sedimentary basin include;

- i. A set of bottom hole temperatures (T_B) are compiled and corrected for drilling disturbances.
- ii. Thermal conductivity values must be measured or determined for all representative rocks in the basin
- iii. Sum the thermal resistance at each well from the surface to the depth of the BHT observation and solve using equation 6 above.

The simple gradient method (Klemme, 1975) is an alternative approach to analysing BHT data. Thermal gradients are calculated as two point differences using a single BHT and an estimate of the mean annual ground temperature or through regression techniques on multiple bottom hole temperatures at different depths (Chapman *et al*, 1984). A major advantage of this method is its convenience. The simple gradient method is given by equation 6 as shown below.

Where, Q is the relative heat flow in Boderij unit (BU), which is equal to $77 \, mWm^{-2}$ in SI unit. *a*, *c*, are constants having values 1.039 and 80.031 respectively,

 T_L, t_L are the subsurface temperature and one-way travel time, respectively, at a deeper depth level of any chosen interval within the well. T_U, t_U , are the temperature and one-way travel time at the shallower depth level of the chosen interval.

The following relations give the geothermal gradient (g_i) and the effective thermal conductivity (k_i) of the interval respectively:

$$g_{i} = \left[\left(T_{L} - T_{L-1} \right) / \left(h_{L} - h_{L-1} \right) \times 100 \right] \quad \dots \tag{9}$$

and $(k_i = 77V/1.039(80.031 + T_i))$ (10)

where h_L , h_{L-1} are the depths (m) corresponding to T_L and T_{L-1} respectively, V, is the acoustic velocity in m/sec.

The velocity of sound waves in a formation can be estimated from a sonic log using the relation:

$$V_{(m/s)} = \left(\frac{1000000}{\Delta t}\right) \times 0.305$$
 (11)

Where Δt is the interval transit time, in $\mu \sec ft^{-1}$, which is read from the sonic log. The one way travel time $t_{(sec)}$ at a particular depth, $Z_{(m)}$ can also be calculated from the following relation:

3.5 Thermal Conductivity Estimation

Thermal conductivity is a physical property describing transfer of heat through the material. The thermal conductivity or rocks is one of the major factors that affect temperatures in sedimentary basins and therefore should be addressed in basin analysis. (Norden and Forster, 2006). Knowledge of thermal conductivity is important in understanding and modelling of the temperature in sedimentary basins Differences in thermal conductivity may affect a basin in such a way that the thermal structure may change laterally and vertically even if heat flow into the basin is regionally the same. In geothermal studies, assessments of thermal conductivities of rocks in an area are either accomplished using the direct measurement or the indirect measurement. Different methods have been used for the direct measurement of thermal conductivity, for which the two main techniques are the stationary divided bar method and the transient needle probe method (Sass et al, 1971 and Brigaud & Vasseur, 1989). The indirect method may be accomplished using one of the wide ranges of formulae based on particle-fluid volume relationship and the corresponding individual thermal properties. (Sass et al, 1971).

Different models of thermal conductivity have been developed (Farouki, 1981; Somerton, 1992). One of the models, the geometric mean model is simple and is used to calculate the thermal conductivity of sediments (Midttomme and Roaldset, 1998). The basic geometric mean equation applied to sedimentary rocks is:

$$k = k_{w}^{\phi} k_{s}^{(1-\phi)}$$
 (13)

Where k is the thermal conductivity of the sample $(Wm^{-1}k)$, k_w is the pore fluid (water) thermal conductivity $(Wm^{-1}k)$, k_w , is the solid matrix conductivity $(Wm^{-1}k)$ and ϕ is the porosity. Two other basic models, the arithmetic and harmonic mean models are also widely used. (Mckenna et al, 1996; Midttomme and Roaldset, 1998). Majorowicz and Jessop (1981) obtained an effective thermal conductivity(k_e) estimates based on net rock analysis and heat conductivity values for different rock types using the following equation;

Where k_i is the conductivity of rock types in a discrete layer I, and d_i , is the thickness of the ith layer.

They showed that their effective thermal conductivity relation could give more reliable results than conductivity estimates based on measured data from only the intervals in which core samples are available. This method is very representative of the whole column of rocks drilled through. In the above equation, the porosity of the rock types, which may contain some fluids, were not considered. Some methods of calculating the effective thermal conductivities that considers the effect of porosity and pore fluids exist. The effective thermal conductivity (k_e) proposed by Huang (1971) is given by the equation;

Where α = the solid δ solid heat transfer coefficient

 β = the fluid ó solid heat transfer coefficient

 $k_s =$ Solid fraction conductivity

$$k_f = fluid$$
 content conductivity

 k_r = radioactive conductivity

The heat transfer coefficient depends on porosity and a geometric factor n, which has a value of zero for pure solids, unity for consolidated porous material and greater than unity for unconsolidated porous material. Beck (1976) proposed a relation that gives an effective thermal conductivity (k_e) for fluid-filled sedimentary rocks drilled through by a well as:

$$k_e = \left[(2r+1) - 2\phi(r-1)/(2r+1) - \phi(r-1) \right] \quad \dots \quad (16)$$

Where $r = k_s/k_f$ = the conductivity ratio; k_s = thermal conductivity of the solid matrix; k_f = the thermal conductivity of the pore fluid; ϕ = the porosity of the sedimentary rock. For very low porosity rocks with small conductivity ratios, the above relation reduces to;

$$k_e = k_s [1 - \phi(r - 1)]$$
(17)

3.6 Transformation of Organic Matter into Hydrocarbons

Three main stages have been recognized in the transformation of organic matter and kerogen. These include; (I) Diagenesis, (II) Catagenesis, (III) Metagenesis

Diagenesis can be divided into early diagenesis and late diagenesis. Early diagenesis includes all the processes that take place prior to deposition and during the early stages of burial, under conditions of relatively low temperature and pressure. The changes here are biological, physical and chemical. Biological agents are mainly responsible for diagenetic transformations. Chemical transformations occur by catalytic reactions on mineral surfaces. Compaction and consolidation takes place here. There is a decrease in water content and an increase in temperature. During this time, biopolymers form.

Biopolymers + CO_2 + H_2O ------(18)

Later Diagenesis is the transformation occurring during and after lithification. Polycondensation takes place here. (i.e. there is a loss of superficial hydrophilic functional groups such as OH and COOH). Geopolymers are created.

Kerogen +
$$CH_4$$
 ------ (19)

End of this phase is marked by a temperature of 60 °C and vitrinite reflectance level (R_0) = 0.6%. R_0 depends on organic matter types. At the end of

diagenesis, sedimentary organic matter is mainly composed of kerogen, which is insoluble in organic solvents.

Catagenesis is a zone in which thermally influenced transformations occur in kerogens. It is temperature dependent and occurs under reducing conditions. The dominant agents are temperature and pressure. It requires minimum temperatures maintained over millions of years and requisite pressure, derived from a few kilometers of overlying rocks and gas pressure as the decomposition of kerogen progresses. Certain characteristics that occur at this stage include;

- the structureless immature kerogen is unstable
- rearrangement of the kerogen structure occurs
- elimination of some groups
- Residual kerogen becomes increasingly compact and aromatic. The loss of aliphatic components and formation of benzene ring compounds through dehydrogenation reactions causes an increase in the aromatic character of kerogen.
- the C ó O and C ó C bonds break to generate and release hydrocarbons, resulting in a decrease in hydrogen content
- H/C and O/C ratios decrease significantly

Hydrocarbon generation during catagenesis can be divided into two zones.

I. The main zone of oil generation (or the oil window) (Table 3.1, Fig 3.1a)

The breakage of C ó O bond in kerogen yields or produces low to medium molecular weight liquid hydrocarbons. As temperature increases, high molecular weight liquid hydrocarbons are first to evolve, after which lower molecular weight hydrocarbons are produced.

II. Wet Gas zone

Thermally induced cracking of C-C bonds in kerogen yields light gaseous hydrocarbons or gas condensate. Gaseous hydrocarbons consist of C_1 to C_5 compounds. C_5 members can be liquids at normal surface conditions. Gas condensate refers to gases from which liquid hydrocarbons condense at the surface during commercial recovery and the liquid is known as condensate.

Metagenesis or Dry gas zone is the zone in which liquid hydrocarbons are cracked at high temperatures to yield dry gas methane and pure carbon (i.e. $CH_4 + C$). The temperature range is > 150 °C and Ro > 2.0%. The wet gas zone and the dry gas zone constitutes the gas window (Table 3.1, Figure 3.1b

Table 3.1: Various stages in the formation of Petroleum hydrocarbons(Frielingsdorf, 2009)

| Stages of Petroleum | | | | |
|---------------------|----------------------------|-----|------------|------------------|
| formation | n Temperature Maturity Vr% | | urity Vr% | Hydrocarbon Type |
| | 0 | 0 | immature | |
| | | 0.2 | immature | biodegredation |
| Diagenesis | 50 | 0.4 | immature | |
| | 60 | 0.6 | oil window | black heavy Oil |
| Catagenesis | | 0.8 | oil window | black Oil |
| | | 1 | oil window | black Oil |
| | | 1.2 | oil window | light Oil |
| | 150 | 1.4 | gas window | volatile oil |
| | | 1.6 | gas window | Condensate rich |
| | | 1.8 | gas window | Dry gas rich |
| | 200 | 2 | gas window | Dry gas |
| Metagenesis | | 2.2 | gas window | Dry gas |
| | | 2.4 | gas window | Dry gas |
| | 240 | 2.6 | overmature | Dry gas |
| | | 2.8 | overmature | Dry gas |
| | | 3 | overmature | |
| | | 3.2 | overmature | |
| | | 3.4 | overmature | |
| | | 3.6 | overmature | |
| | | 3.8 | overmature | |
| | | 4 | overmature | |

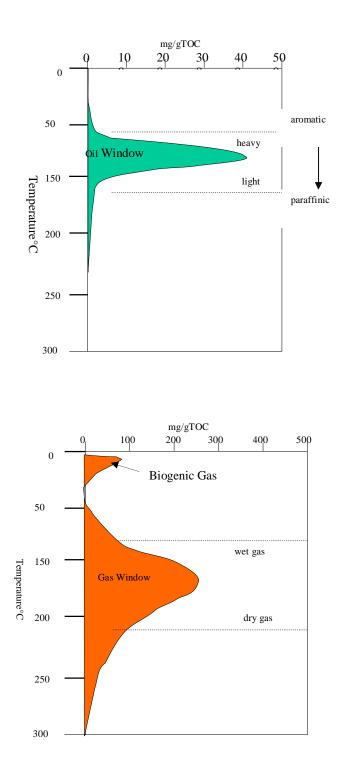


Fig. 3.1: (a) The oil window and (b) the gas window(Frielingsdorf, 2009)

3.7 Time and Temperature: kinetics of maturation

The nature of organic matter and its thermal history determines the maturation of kerogen into hydrocarbons (Tissot and Welte, 1984). According to Connan (1974) and Pigott (1985), the most important factors influencing organic matter maturation include amount and type of organic matter, temperature, time as well as pressure.

The effects of time and temperature on thermal reactions occurring in sediments during burial are first order reactions which obey the Arhenius equation, describing the intensive variable K as:

 $K = A \exp (-E / RT)$ ------ (21) Where K is the rate constant, A is the frequency factor, E is the activation energy, R is the universal gas constant (joule mole ⁻¹K⁻¹) and T is the temperature.

In order to quantify the amount of evolved oil and gas, it is necessary to determine the constants and specify T. The Time ó Temperature Index (TTI) method of calculating maturity as used by Lopatin (1971) and Waples (1980) as well as the classic level of organic metamorphism (LOM) of Hood et al (1975) are all applications of Arhenius equation used to quantify the time ó temperature dependency on source rock maturity.

The model used in this study utilizes a broad distribution of Arhenius rate constants to calculate vitrinite maturation, then correlates maturation with reflectance. Sweeney and Burnharmøs Easy % kinetic model of calculating source rock maturity was used in this study which correlates the oil window for mixed type II / III kerogen.

3.8 Thermal Maturity Modelling

Basin modelling is a powerful tool for the evaluation of the temperature and maturity evolution and hence petroleum generation and migration from potential source rocks in sedimentary basins (Tissot et al, 1987). It is an integrated study that takes into account all geological, geophysical and geochemical processes that takes place during the entire geological history of the basin. Maturity modelling is a major part of basin modelling. Maturity models are used in describing the behaviour of individual thermal indicators with regard to hydrocarbon generation of potential source rocks. Maturity modelling can be described as the simulation of geohistory, thermal history and hydrocarbon generation.

3.7.1 Burial History Analysis

Burial History is a term used to describe plots showing the depth of burial of a given sedimentary formation as a function of post-depositional time (Seiver, 1983). It also shows the changes that take place in the sedimentary section as well as the gradual thinning of each formation in accordance to its assumed rate and extent of compaction. Geohistory analysis is another term that is often used to describe burial history (subsidence and uplift) and related processes like decompaction / compaction and the analysis of removed sections. Geohistory analysis quantifies subsidence and sediment accumulation / erosion through time of a well section or an outcrop section. A geohistory diagram is used to analyse the subsidence history of a surface point in relation to its present day elevation.

3.7.2 Thermal History

Thermal History is the expression of the temperature intensive property as it varies through time and its determination is very vital to both maturity and kinetic calculations (Metwalli and Pigott, 2005). Thermal history is a very important aspect of basin modelling, as the maturity and generation of hydrocarbon are mainly dependent on temperature. Temperature and time are utilised in thermal history modelling of a sedimentary basin. Temperature is used in determining the maturity and generation level whereas time is used for the charge history of the structural traps. Thus a reconstruction of the heat flow evolution over time and the change in geothermal gradient with time and depth is necessary. This is done by setting boundary conditions which includes:

- Basal Heat Flow (HF) ó lower thermal boundary
- Paleo water depth (PWD) or upper thermal boundary
- Sediment water interface temperature (SWIT) ó upper thermal boundary

The boundary conditions define the basic conditions for the temperature development of all layers, especially the source rock and, consequently for the maturation of organic matter through time. With these boundaries and the thermal conductivity of each lithology, a paleotemperature profile can be calculated at any event.

3.7.3 Heat Flow Estimation

It is important to know the heat flow history of a sedimentary basin in order to assess the generative potential of kerogens as well as the amount and timing of the petroleum generated in the sedimentary rocks. The heat flow history is usually derived from geological consideration and only heat flow values at maximum burial and present day are useful for thermal maturity modelling.

For the reconstruction of thermal histories and the evaluation of source rock maturation and petroleum generation, a corresponding heat flow history has to be assigned to the geological evolution. The paleo heat flow is an input parameter. . Basins affected by crustal thinning and rifting processes (Mckenzie 1978, Jarvis and Mckenzie, 1980, Allen and Allen 1990) usually experience high heat flows during the basins initiation. Iliffe et al (1999) as well as Carr and Scotchman (2003) also attest to the fact that elevated heat flows are required for rifting events and such a model is preferred to the constant heat flow model. The finite rifting model is thus the most widely accepted theory and the general model involves two phases:

(I) rifting phase: stretching, thinning and faulting of the crust accompanied by increased heat flow due to upwelling of the asthenosphere;

(II) subsidence phase: post rift exponential thermal decay owing to re-establishment of thermal equilibrium in the mantle, lithosphere and asthenosphere.

3.7.4 Geochemical Parameters

Geochemical parameters that are specified for each source rock interval include:

- The total organic carbon (TOC) content
- The Hydrogen Index (HI) and
- The Kerogen kinetics

The ability of a potential source rock to generate and release hydrocarbons is dependent upon its contents of organic matter, which is evaluated by total organic carbon (TOC) content, expressed as weight percentage organic carbon (Hunt, 1996) The total organic carbon content and Rock eval pyrolysis data specifies the quantity and quality of organic matter available within the source rocks. This information is used for calculation of generated hydrocarbons that have been transformed from organic matter in the source rock. Peters (1986) has shown that TOC can be used to describe potential source rocks as shown in table 3.2.

Rock eval pyrolysis, was developed by Espitalie et al (1977) and is commonly used to determine the hydrocarbon generative potential of organic matter. A flame ionization detector (FID) senses any organic compounds generated during pyrolysis. The measured parameters include S1; free hydrocarbons present in the rock that volatized at a moderate temperature, S2; the hydrocarbons generated by pyrolytic degradation of the kerogen and S3; oxygen ó containing volatiles, i.e., carbon dioxide Another important parameter is the temperature, known as Tmax, and water. corresponding to the maximum of hydrocarbon generation during pyrolysis. Kerogen types are characterized using two indices; the hydrogen index (HI = $S2 \times 100 / TOC$) and the oxygen index (OI = S3 \times 100 / TOC). The indices are independent of the abundance of organic matter and are strongly related to the elemental composition of kerogen. The organic matter type or the kerogen type can be distinguished by plotting the oxygen index against the hydrogen index. This is known as the Van Krevelen diagram. Peters (1986) has also shown that using the hydrogen index (HI) the following products (gas + oil) will be generated from source rocks at a level of thermal maturation equivalent to $R_0 = 0.6\%$. (Table 3.3)

| TOC (Wt. %) | Source rock quality |
|-------------|---------------------|
| <0.5 | Poor / non source |
| 0.5 ó 1 | Fair / Marginal |
| 162 | Good |
| 2 - 4 | Very Good |
| > 4 | Excellent |

Table 3.2: Using TOC to assess the source rock generative potentials (Peters,1986)

Table 3.3: Using the Hydrogen index to assess the type of hydrocarbon generated(Peters,

1986)

| HI | (mg HC/gC _{org}) | Source potential |
|----|----------------------------|-------------------|
| | 0 - 150 | Gas |
| | 150 - 300 | Mixed (Oil + Gas) |
| | 300+ | Oil |

CHAPTER FOUR

4.0 DATA ANALYSIS

4.1 Basic Data Used

The basic data used for this study include;

1. Temperature data sets, such as:

(i) Bottom - hole temperatures (BHT) measurements taken during logging runs.

(ii) Production reservoir températures

(2) Stratigraphic and biostratigraphic age data; given as MFS (Maximum Flooding Surfaces) and SB (Sequence Boundary)

- (3) Sand percentages
- (4) Porosity logs, such as the sonic log

4.1.1 Collection and Analysis

The bottom-hole temperature (BHT) data were sourced from well logs. The reservoir data were obtained from ARPR (Annual Review of Petroleum Resources) data file, the shell database, Petrotrek, and well file reports in the Shell Library. Continuous temperature temperatures data were collected from Petrotrek. The continuous temperature logs from Petrotrek were not used because they were recorded when the temperatures have not stabilized from drilling perturbations and as such are not close to static formation temperatures. The lithologic, biostratigraphic, sand percentages data, as well as porosity logs were also obtained from the Petrotrek file.

4.1.2 Analytical Software

Softwares used include Excel, Petromod 1D basin modelling package), ArcGIS and Petrel (a mapping software).

4.2 Temperature Data

The temperature data used are mainly reservoir and corrected bottom-hole temperature data.

4.2.1 Temperature Corrections

Reservoir temperature data and corrected bottom-hole temperature data were used to characterize the thermal regime of parts of the Eastern Niger Delta. Reservoir temperatures are noted as providing direct measurements of temperatures at depth that are fairly reliable. (Husson *et al*, 2008a). Bottom-hole temperatures data are usually acquired before thermal equilibrium was reached. Empirical (Bullard, 1947, Horner, 1951) and statistical (Deming and Chapman, 1988) correction techniques exist, but they require some information that is not available, such as circulation time and shut in time (Table 4.1 and Appendix 1). In this study the routine technique generally used for hydrocarbon exploration purpose was adopted due to the general lack of data. The equilibrium or static formation temperature was therefore calculated by simply increasing the BHT by 10% ΔT

Where $\Delta T = T_b - T_s$ ------ (21)

and T_b is the temperature at depth while T_s is the surface temperature, which is assumed as 27°C and 22 °C for the Central and Coastal swamps as well as the Shallow Offshore respectively. This technique was used by Husson *et al* (2008a) for correcting BHT data in the north-western part of the Gulf of Mexico.

4.2.2 Temperature Scales and Conversion Factors.

All the data used were originally recorded in Fahrenheit scale but were converted in this study to the Celsius scale. The Fahrenheit scale has a fundamental interval of 180 °F. It starts from 32 °F and ends at 212 °F. The Celsius scale starts from 0 to 100 °C, having an interval of 100 °C.

The conversion scales used for conversion of Fahrenheit to Celsius and viceversa is given as follows:

$$C = (F - 32) \times \frac{5}{9}$$
(22)
$$F = C \times \frac{9}{5} + 32$$
(23)

| | | | OTTOM HOLE TE | Shut | | | | | |
|-----|----------------|-----------------------------|--------------------------|------------|---------|-----------|---------|----------|------|
| S/N | Well Names | Time circulation stopped | Time logger on bottom | in time | BHT(oF) | Depth(FT) | BHT(oC) | Depth(m) | BHT© |
| | | | | | | 0 | | | |
| 1 | Abak - Enin -1 | | 30/08/1975 | 2 | 140 | 4520 | 60 | 1483 | 63 |
| | | 10-9-75/06:00 | 10-9-75/10:00 | 4 | 164 | 9010 | 73.33 | 2956 | 78 |
| | | | 10/9/1975 | 6 | 164 | 9010 | 73.33 | 2956 | 78 |
| | | | 10/9/1975 | 9 | 164 | 9010 | 73.33 | 2956 | 78 |
| | | | 10/9/1975 | 13 | 164 | 9010 | 73.33 | 2956 | 78 |
| | | | 10/9/1975 | 16 | 164 | 9010 | 73.33 | 2956 | 78 |
| | | 20/09/75/14:00 | 20-9-75/20:00 | 6 | 184 | 9438 | 84.44 | 3096 | 90 |
| | | | 22/09/1975 | 5 | 168 | 9408 | 75.56 | 3087 | 80 |
| | | | 22/09/1975 | 8 | 168 | 9408 | 75.56 | 3087 | 80 |
| | | | 22/09/1975 | 10 | 168 | 9408 | 75.56 | 3087 | 80 |
| 2 | Ajokpori-1 | | 19/02/1967 | | 108 | 4005 | 42.22 | 1314 | 44 |
| | | | 3/3/1967 | | 171 | 10837 | 77.22 | 3555 | 82 |
| | | | 5/3/1967 | | 173 | 11235 | 78.33 | 3686 | 83 |
| 3 | Akai-1 | 18-4-87/20:30 | 14-4-87/06:20 | | 132 | 5018 | 55.56 | 1646 | 59 |
| | | 02/05/87/22:15 | 3-5-87/10:30 | | 179 | 8697 | 81.67 | 2853 | 88 |
| | | 02/05/87/22:15 | 3-5-87/13:12 | | 179 | 8697 | 81.67 | 2853 | 88 |
| | | 5/13/1987 | 13-5-87/23:30 | | 195 | 9198 | 90.56 | 3018 | 97 |
| | | 16-5-87/22:00 | 19-5-87/09:54 | | 209 | 9943 | 98.33 | 3262 | 105 |
| 4 | Akaso-4 | | | | | | | | |
| 5 | Akata-1 | | 12/4/1953 | | 102 | 4065 | 38.89 | 1334 | 40 |
| | | | 4/6/1953 | | 150 | 7000 | 65.56 | 2297 | 70 |
| | | | 2/7/1953 | | 160 | 8185 | 71.11 | 2685 | 75 |
| | | | 22/07/1953 | | 239 | 10787 | 115 | 3539 | 124 |
| | | | 7/10/1953 | | 245 | 11104 | 118.3 | 3643 | 127 |
| | | | 7/10/1953 | | 245 | 11111 | 118.3 | 3645 | 127 |
| | | 13-09- | | | | | | | |
| 6 | Akikigha-1 | 1987/13:00 | 13-9-87/18:41 | 5:41 | 112 | 5002 | 44.44 | 1641 | 46 |
| | | 25-9-87/03:00 | 25-9-87/20:30 | 17:30 | 159 | 9000 | 70.56 | 2953 | 75 |
| | | 25-9-87/03:00 | 25-9-87/15:45 | 12:45 | 156 | 9012 | 68.89 | 2957 | 73 |
| | | 25-9-87/03:00 | 25-9-87/10:00 | 7 | 154 | 9001 | 67.78 | 2953 | 72 |
| | | 25-9-87/03:00 | 26-9-87/00:15 | 21:15 | 163 | 9008 | 72.78 | 2955 | 78 |
| | | 5-10-87/17:00 | 6-10-87/04:00 | 12 | 187 | 10455 | 86.11 | 3430 | 72 |
| | | 25-9-87/03:00 | 26-9-87/02:30 | 11:30 | 232 | 14234 | 111.1 | 4670 | 109 |
| | | 25-9-87/07:45 | 26-9-87/02:30 | 6:45 | 232 | 14234 | 111.1 | 4670 | 109 |
| | | 5-10-87/17:00 | 6-10-87/14:15 | 21:15 | 194 | 10464 | 90 | 3433 | 96 |
| | | 5-10-87/17:00 | 6-10-87/09:00 | 16 | 191 | 10468 | 88.33 | 3434 | 94 |
| 7 | Akuba-1 | | 12/2/1967 | | 172 | 10380 | 77.78 | 3406 | 83 |

4.2.3 Determination of Geothermal Gradients

The basic equation for the determination of geothermal gradients as given by Bradley (1975) is as follows:

Geothermal Gradient =
$$\frac{T_d - T_s}{X} \times 1000$$
 -----(24)

Where T_d and T_s are temperatures below and at the surface respectively, while X is the formation depth. The temperatures are in degrees Celsius and depth is given in meters and the thermal gradient is in degrees Celsius per kilometre ($^{\circ}C/Km$).

4.2.3.1 Mean Annual Surface Temperature

A good knowledge of the surface temperature is important in the determination of the geothermal gradient in a sedimentary basin because the surface temperature provides a boundary condition. The mean annual surface temperature is an approximation of the temperature at the air-sediment boundary. Accordingly, an equilibrium surface temperature of 27 °C (80 °F) was used for the Central Swamp and the Coastal Swamp. A seabed surface (i.e. mudline) temperature of 22 °C was also applied to the Shallow Offshore. In offshore areas, because of the intervening water column, the air temperatures does not truly reflect temperature at the top of the sediment column and therefore may give spurious results in geothermal gradient calculations. The mean air temperature at the water surface in the deep offshore is considerably higher than the seabed or mudline temperature. The seabed temperature was used as the surface temperature because the depths to the seabed surface for these shallow offshore wells range from 17 to 50m and therefore shows no significant change of temperature with water depth. Figure 4.1 is a simple temperature-depth ocean water profile for low to middle latitudes, which shows how temperature decreases with increasing water depth. This figure was obtained from the web site; http://www.windows.ucar.edu/tour/link=/earth/water/images/temperature_depth_jpg

i . This is corroborated by Figure 4.2, showing bottom water temperature as a function of water depth obtained by Brooks *et al* (1999) at heat flow measurement sites, offshore Nigeriaøs continental margin. In offshore areas, the geothermal gradients are usually calculated using mud-line temperature as the surface temperature. The mud-line is usually determined from the temperature-depth ocean water profile as the water depth at which the field or well is located. (Figure 4.1)

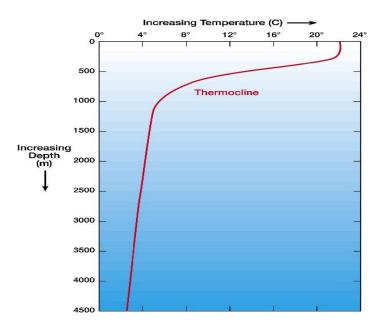


Fig. 4.1: A simple temperature- depth ocean water profile (from http:// www.Windows.ucar.edu.tour/link=/earth/Water/temp.htm&edu=high

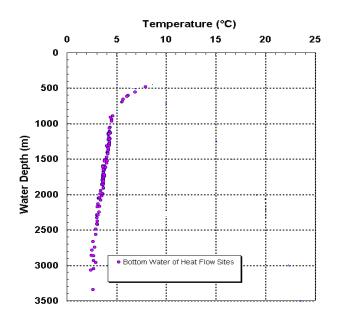


Fig. 4.2; Bottom water temperature as a function of depth, at heat flow sites on Nigeria's offshore continental margin (Brooks et al, 1999)

4.2.3.2 Methodology

Two models were utilized in studying the geothermal gradient patterns in parts of the Eastern Niger Delta. These include;

(i) A constant geothermal gradient model

(ii) A variable geothermal gradient model

In the first model, a single linear regression of temperature versus depth is considered as a convenient first order approximation (Appendix II) while in the second model, the temperature-depth data sets are well fit by two constant gradients at depth (Appendix III). In this model an upper or shallow thermal gradient and lower or deeper thermal gradient were determined. In this case, a sharp break in thermal gradient occurs at depth. This will give a considerable better fit than that given by a single linear regression.

To calculate geothermal gradients, reservoir temperature (RT) and (BHT) data from each well was loaded into an excel spreadsheet. The BHT depth data was then converted to a true vertical depth (TVD óSS) using directional survey data from log headers. The Reservoir temperature data from ARPR file had already been converted to a sub-sea true vertical depth. An excel macro was used to plot data from each well, field and depobelt on a temperature-depth graph. Each plot was examined and a gradient line or series of gradient lines was visually established and drawn through the points. The mean annual surface temperature at the air-sediment interface and the temperature at the seabed-water interface (i.e. the mud-line) were used as the shallowest point. For each of the well data, after establishing the gradient lines, values were extracted from each plot to calculate a gradient and the 100°C and 150°C isotherm depth. If dogleg gradients are observed, the temperature of the deepest point, above the deepest dogleg was recorded, and the gradient of this last step was used to calculate the temperatures at 1000m, 2000m, 3000m and the depth at which temperatures of 100°C and 150°C were attained.

4.2.4 Temperature and Geothermal Gradient Mapping

The temperature field in a linear regression (i.e. average geothermal gradient model), were computed using the following relation:

$$T_{(z)} = Z_{g} + T_{s}$$
(25)

Where Z is the formation thickness, g is the geothermal gradient and T_s , is the seabed or surface temperature.

In the second case, (i.e. variable geothermal gradient model), temperatures were well fit by two constant geothermal gradients. Temperatures are thus computed using the following equation:

 $T_{(z)} = T_s + g_1 z + g_2 (z - z_0)$ (26)

Where g_1 is the upper thermal gradient, g_2 , is the lower thermal gradient, z_0 is the rupture depth and z is the formation thickness.

The estimated temperatures may also be presented in temperature maps showing the temperature fields at specific depths of 1000m, 2000m, and 3000m. An alternative way to examine the temperature-depth relationship is the isothermal maps. Isothermal maps involve mapping the depth to a constant temperature such as 100°C and 150°C. Geothermal gradient maps can also be presented as average geothermal gradient map and geothermal gradient map of the shallow section (continental sandstones) and for the deeper marine/paralic section. These maps were contoured using Petrel 2007 software.

4.3 Sand and Shale Percentages

4.3.1 Method of Determination

Sand and Shale Percentages are usually determined from gamma ray logs, resistivity and spontaneous potential logs. For this study, the sand and shale percentages for all the wells were retrieved from the shell database known as Petrotrek.

4.3.2 Sand Percentage Mapping

The sand percentage data were averaged for certain depth intervals such as: $0 \circ 4000$ ft ($0 \circ 1312$ m) and $4000 \circ 9200$ ft ($1312 \circ 3000$ m) for each of the wells. The average sand percentages for all the entire project area were then contoured using Petrel 2007 software.

4.4 Thermal Maturity Modelling

In this work, PetroMod 1-D modelling software package (Version 11, 2009) made by IES Germany were used to reconstruct the burial and thermal history,

evaluate the hydrocarbon potentials as well as the timing of petroleum generation across the Coastal Swamp, the Central Swamp and Shallow Offshore of the Eastern Niger Delta.

4.4.1 Burial History Analysis

4.4.4.1 Model Construction

According to Underdown and Redfern (2007), the conceptual model used in basin modelling is derived from the geological evolution of the basin under consideration and is thus based on the geological framework of the study area. This therefore gives the temporal framework that is required to structure the input data for computer simulation. Stratigraphic analysis provides one of the most important inputs to the conceptual model. The sedimentation history is then subdivided into a continuous series of events, each with a specified age and duration of time. Each of these stratigraphic events represents a time span during which deposition (sediment accumulation), non-deposition (hiatus) or uplift and erosion (unconformity) occurred. The model for the Niger Delta basin used in this study contains a maximum of 7 events (layers) and is summarized in tables 5.09, 5.10, 5.11, 5.12. Models were constructed from Paleocene (65 Ma) to Recent.

4.4.1.2 Input Parameters

In order to carry out a burial history reconstruction the following input data are required.

- Depositional thickness
- Depositional age in Ma (millions of years)
- Lithological Composition
- Thickness and age of eroded intervals
- Petroleum Systems Essential Elements (Underburden, Source Rocks, Reservoir rocks, Seal Rock and Overburden rock
- Possible source rock properties (TOC & HI)
- Applicable kinetics

Depositional thicknesses and absolute ages in many of the different stratigraphic units were defined using biostratigraphic data and Shell Development Company of Nigeria Limited Cenozoic Geological data table (Table 4.2). A generalised stratigraphy and tectonic history of the Niger Delta and the Benue Trough is shown in table 4.3. The thicknesses of sedimentary layers not penetrated by wells were estimated from available data from surrounding wells (Table 4.4). The lithological composition of the stratigraphic units was obtained from the sand/shale percentage data. The petrophysical properties of the lithologies were provided by the modelling package.

4.4.2 Thermal History

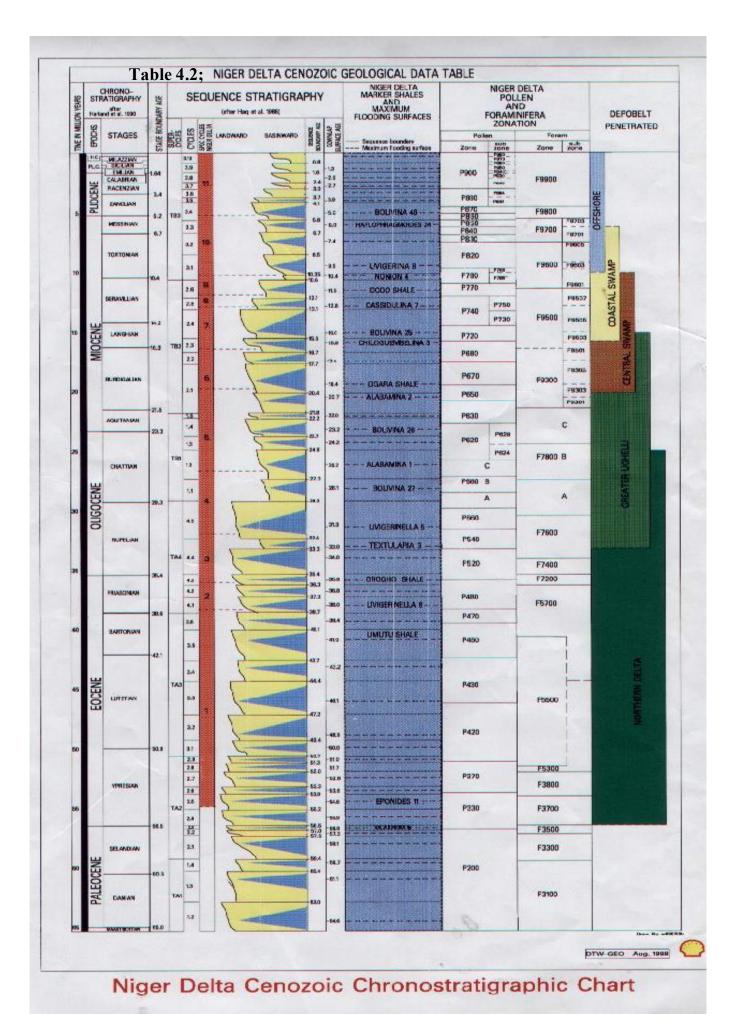
Thermal History is the expression of the temperature intensive property as it varies through time and its determination is very vital to both maturity and kinetic calculations (Metwalli and Pigott, 2005). Thermal history is a very important aspect of basin modelling, as the maturity and generation of hydrocarbon are mainly dependent on temperature. Temperature and time are utilised in thermal history modelling of a sedimentary basin. Temperature is used in determining the maturity and generation level whereas time is used for the charge history of the structural traps. Thus a reconstruction of the heat flow evolution over time and the change in geothermal gradient with time and depth is necessary. This is done by setting boundary conditions which includes:

- Basal Heat Flow (HF) ó lower thermal boundary
- Sediment water interface temperature (SWIT) ó upper thermal boundary

The boundary conditions define the basic conditions for the temperature development of all layers, especially the source rock and, consequently for the maturation of organic matter through time. With these boundaries and the thermal conductivity of each lithology, a paleotemperature profile can be calculated at any event.

4.4.3 Paleobathymetry

The paleobathymetry or the paleo-water depth (PWD) data are used to reconstruct the total subsidence that has occurred within a basin. Paleobathymetry is used for subsidence calculation and to display burial curves with respect to sea level. It has no influence on the temperature and geochemical calculations. The estimated values of paleobathymetry for the Niger Delta used in the models are shown in table 4.5



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 Table 4.3: Generalized Stratigraphy and Tectonic History of the the Tertiary Niger Delta.

| Location | Source rock | Top depth | Bottom depth (m) | Thickness(m) |
|------------------|---------------|-----------|------------------|--------------|
| | name | (m) | | |
| Nsit -1 | Oligocene | 1207 | 2146 | 939 |
| | L. Eocene | 2146 | 2264 | 118 |
| | Paleocene | 2264 | 2412 | 148 |
| Etinan -1 | Miocene | 1129 | 1568 | 459 |
| | Oligocene | 1568 | 2297 | 729 |
| Midim -1 | Miocene | 328 | 1175 | 847 |
| | Oligocene | 1175 | 2920 | 1745 |
| | U. Eocene | 2920 | 3076 | 156 |
| Edik - 1 | L. Miocene | 411 | 556 | 145 |
| | Oligocene | 556 | 639 | 83 |
| | Eocene | 639 | 957 | 318 |
| | Palaeocene | 957 | 1812 | 855 |
| Akaso | U. Eocene | 5300 | 6000 | 700 |
| | L. Eocene | 6000 | 7000 | 700 |
| | Palaeocene | 6700 | 7400 | 700 |
| Uge ST | Oligocene | 3410 | 4220 | 810 |
| | U.Eocene | 4220 | 5401 | 1181 |
| Summary | | | | |
| Estimates | | | | 1 |
| Source rock name | Thickness (m) | | | |
| L.Miocene | 340 | | | |
| Oligocene | 842 | | | |
| Eocene | 635 | | | |
| Paleocene | 568 | | | |

Table 4.4: Model used to estimate the thickness of the Miocene, Oligocene, Eocene and the Palaeocene sediments.

| Epoch | | Age | Water Depth | |
|-----------|--------------|-------|-------------|--|
| Holocene | | 0 | 0 | |
| Pliocene | Placencian | 3.6 | 30 | |
| | Zanclean | 5.33 | 10 | |
| Miocene | Serravillian | 13.82 | 150 | |
| | Langhan | 15.97 | 300 | |
| Oligocene | | 33.9 | 100 | |
| Eocene | | 48.6 | 80 | |
| | | | | |

Table 4.5: Paleobathymetry of sediments in the Niger Delta as used for input in the modelling

4.4.4 Heat Flow

It is important to know the heat flow history of a sedimentary basin in order to assess the generative potential of kerogens as well as the amount and timing of the petroleum generated in the sedimentary rocks. The heat flow history is usually derived from geological consideration and only heat flow values at maximum burial and present day are useful for thermal maturity modelling.

For the reconstruction of thermal histories and the evaluation of source rock maturation and petroleum generation, a corresponding heat flow history has to be assigned to the geological evolution. The paleo heat flow is an input parameter, which is commonly difficult to define. Following published concepts on heat flow variations, basins affected by crustal thinning and rifting processes (McKenzie 1978, Allen and Allen 1990) usually experience elevated heat flows during the basins initiation. For all simulations the scenario adopted is thus; a steadily increasing heat flow history from a value of 60 mWm⁻² at 125Ma. A maximum heat flow value of 90 mWm⁻² was assigned for the heat flow experienced at 85Ma, the break-up phase of the basins initiation (Figure 4.3). Assuming a gradual cooling, as proposed by theoretical stretching models (Mckenzie, 1978), the heat flow then declines to its lower present day values. The present day heat flow is then adjusted until the calculated present day temperature field fits the observed thermal structure constructed from well log temperature measurements. To match present-day heat flow, as calibrated against temperature data, lower heat flow values of c. 29 ó 55 are needed.

4.4.5 Calibration Parameters

In this study, corrected bottom-hole temperatures (BHT) and reservoir temperatures (RT) were used for the calibration of the temperature history of the basin. The measured temperature values were compared with calculated temperature values. The model uses the Easy% Ro algorithm of Sweeney and Burnham (1990) to calculate vitrinite reflectance. This is the most widely used model of vitrinite reflectance calculation and is based on a chemical kinetic model that uses Arhenius rate constants to calculate vitrinite elemental composition as a function of temperature. No vitrinite reflectance data were made available. The results of the simulation include a calculated Easy $% R_0$ of Sweney and Burham (1990).

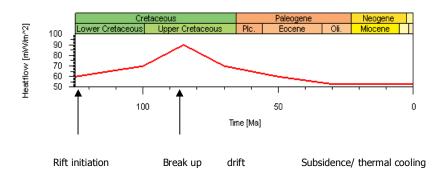


Fig. 4.3. Heat flow history model of the Niger Delta used in the present study

4.4.6 Petroleum Geochemistry

4.4.6.1 Organic matter content and quality

The geochemical and petrologic characteristics of organic matter provide data that must be considered in evaluating potential source rocks (Bustin, 1988). The total organic carbon content (TOC) and rock-eval pyrolysis measurements gives information on quality and quantity of organic matter. This information is used for calculation of hydrocarbons that have been transformed from organic matter in the source rocks. TOC and rock-eval pyrolysis data were not given for any particular well. However TOC and rock eval data exists in literature for most of the stratigraphic units in the Niger delta, and also for older Tertiary and Cretaceous rocks of the adjacent Anambra Basin and the Benue Trough. The geochemical evaluation used in this study is based on geochemical data available in literature (Bustin, 1988; Udo and Ekweozor, 1988; Ekweozor and Okoye, 1980, Ekweozor and Daukoru, 1994) as well as from some confidential records. The average source rock values for the various stratigraphic units in the Niger Delta are given in table 4.6. For the modelling study, the Upper Miocene, Lower Miocene, Oligocene, Eocene and Palaeocene are considered as effective source rocks. For the calculation of kerogen transformation, the kinetic dataset of Burnham (1989) for type II / III kerogen was used.

A marked decrease in total organic carbon content occurs in the source rocks of the Niger Delta from a mean of 2.2% in late Eocene strata to 0.90% in Pliocene strata.(Bustin, 1988). Udo and Ekweozor (1988) similarly has obtained an average TOC of 2.5% and 2.2% for the Agbada - Akata shales in two wells in the Niger Delta. The variation of the total organic carbon (TOC) with age is shown in figure 4.4a. The total organic carbon (TOC) content is thus greater in Upper Eocene to Oligocene strata, followed by lower and middle Miocene and Upper Miocene ó Pliocene strata. Organic petrography suggests that the organic matter consists of mixed maceral components (85 ó 98%) vitrinite with some liptinite and amorphous organic matter (Bustin, 1988). There is no evidence of algal matter.

| Epoch | TOC (%) | HI(mgHCg ⁻¹ TOC | Kerogen type |
|----------------|-------------|----------------------------|--------------|
| Pliocene | 0.87 -0.90 | 50 - 55 | III / IV |
| Upper Miocene | 0.80 ó 0.85 | 57 ó 60 (100) | II / III |
| Middle Miocene | 1.2 ó 1.3 | 70 ó 75 (100) | II / III |
| Lower Miocene | 1.4 ó 1.5 | 60 ó 80 (100) | II / III |
| Oligocene | 1.6 - 1.7 | 85 -100 (150) | II / III |
| Eocene | 1.8 ó 2.3 | 72 ó 100 (250) | II / III |
| Paleocene | 2.5 | (350) | II / III |

Table 4.6: Source rock properties of Tertiary sediments of the Niger Delta (Compiled from Bustin, 1988 and Confidential data)

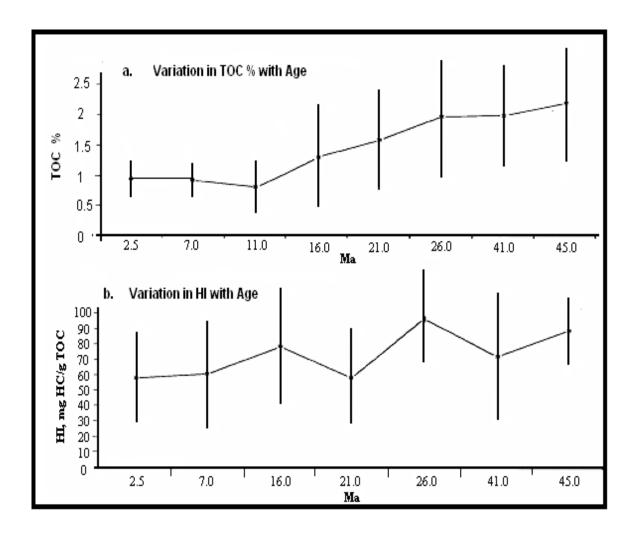


Figure 4.4: (a) Variation in TOC content with age for strata with less than 10% TOC (n = 1221).(b) Variation in HI with age for strata with less than 10% TOC (n = 616) (After Bustin, 1988

Bustins (1988) rock eval pyrolysis result suggests that the hydrogen indices (HI) are quite low and generally range from 160 to less than 50mgHC/gTOC. There is also a general decrease in hydrogen index from the Eocene strata to the younger Pliocene sediments (Figure 4.4b), although not as significant as TOC. In Ekweozor and Daukoru (1994) view, an average hydrogen index value of 90 mgHC/gTOC suggested by Bustin (1988) is an underestimation of the true source rock potential because of the matrix effect on whole rock pyrolysis of deltaic rocks. Bustins plot of rock eval determined oxygen index (OI) and hydrogen index (HI) on a Van-krevelan-type (HI/OI) diagram shows that almost all samples plot between type II and type III kerogen (Figure 4.5). Similarly Lambert-Aikhionbare and Ibe (1984) has shown in their elemental analysis (carbon, hydrogen, nitrogen and oxygen) of the kerogens that the kerogen type is mainly type II with varying admixtures of type I and III. (Fig. 4.6)

In general, no rich source rock occurs in the Tertiary succession of the Niger Delta and as conventionally measured; the strata have little or no oil generating potential. According to Bustin (1988), the poor quality of the source rocks has been compensated for by the great volume of the source rocks, the excellent migration routes provided by interbedded permeable sands and the relatively high rate of maturation.

4.4.7 Thermal Conductivities of sediments in the Niger Delta

The sediments in the Niger Delta principally consist of sands and shales in variable proportions. The thermal conductivities of these deltaic sediments generally decreases with depth, varying in the following manner; 1.81 ó 2.26 W/mK for sands, 1.63 ó 2.19 W/mK for shaly sands, 1.56 ó 1.76 W/mK for shales, 1.85 ó 1.95 W/mK for sandy shales and 2.04 ó 2.15 W/mK for equal proportions of shale and sand. The thermal conductivities of these prominent lithologies in the Niger Delta shows a wide variation from well to well. Plots of thermal conductivities and lithology as a function of depth for some wells in the Niger Delta are shown in figures 4.7 a ó d.

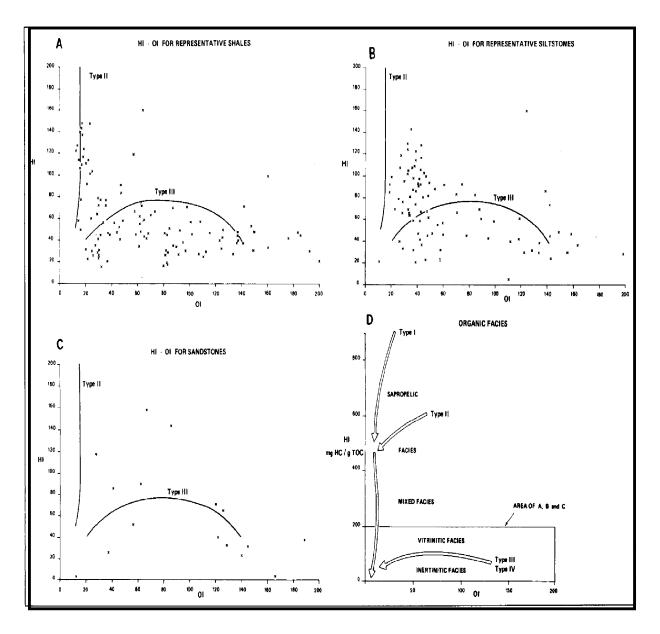


Figure 4.5: HI/OI diagram for (a) Shales (includes all clay rocks); (b) Siltstones; (c) Sandstones; (d) chemical facies diagram (Bustin, 1988)

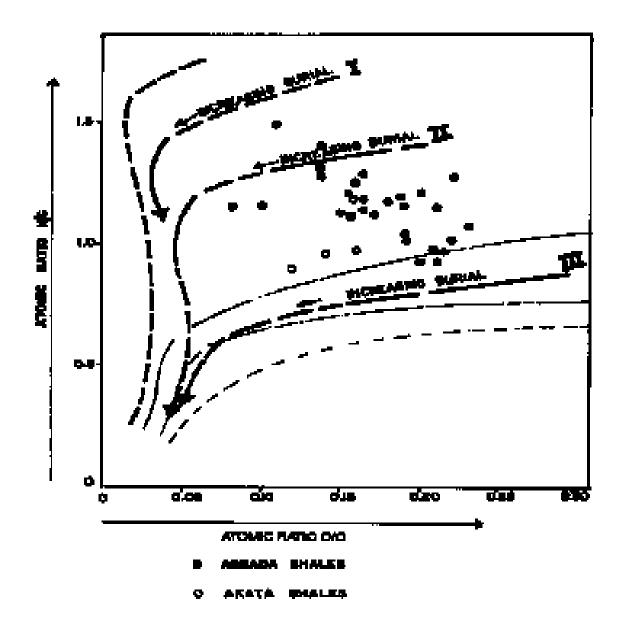


Figure 4.6: Van Krevelens diagram with results of elemental analysis of some kerogen of Agbada and Akata shales of the Niger Delta (Lambert-Aikhionbare and Ibe, 1984)

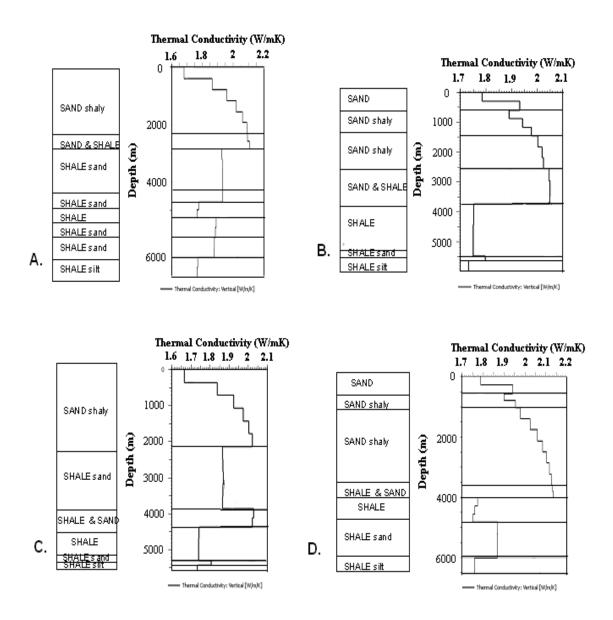


Figure 4.7: Thermal coductivity variations in (a) Akaso – 4 (b) Obigbo – 1 (c) Opobo South – 4 and (d) Kappa – 1 wells in the Niger Delta.

4.4.8 Sedimentation Rates in the Niger Delta

Sedimentation rates (VSE) is usually calculated by dividing the actual thickness (Z_2) of the sedimentary layer by the difference between the age of the bottom and top of the layer.

| Sedimentation rate VSE = Z_2 / T | (27) |
|------------------------------------|------|
| Where $T = t_2 - t_1$ | (28) |

Sedimentation rates were calculated for Pliocene to Recent sediments in the study area. The result shows that sedimentation rates are highest in the Shallow Offshore and in the western part of the Coastal Swamp (Fig. 4.8). Sedimentation rates in the Shallow Offshore ranges from 200 ó 700 m/Ma while in the western part of the Coastal Swamp it ranges from 100 ó 500 m / Ma. In the Central Swamp and the Eastern parts of the Coastal Swamp, the sedimentation rates vary between 100 ó 300 m / Ma.

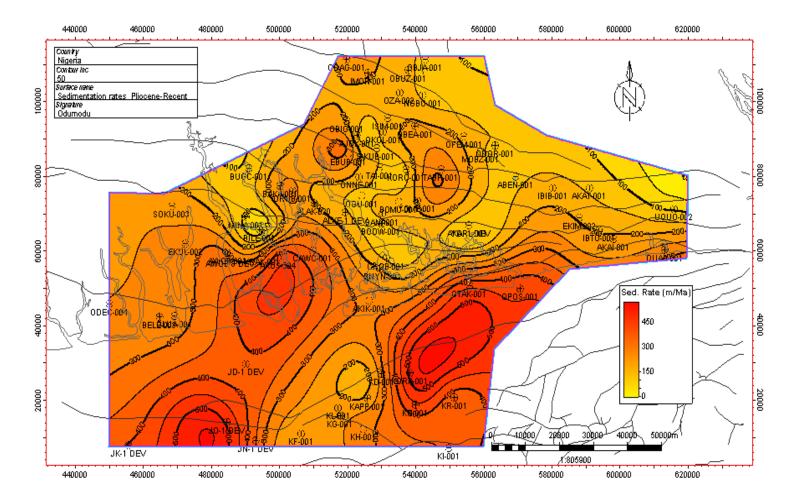


Figure 4.8: Map showing variations in Sedimentation Rates for Pliocene to Recent sediments in the Niger Delta

CHAPTER FIVE

5.0 RESULTS AND INTERPRETATION

5.1 Geothermal Gradients

Geothermal gradients pattern in the eastern part of the Niger Delta were determined using reservoir and corrected bottom-hole temperatures data. The result shows that the Central and Coastal Swamps were characterized by two-leg dogleg geothermal gradients pattern whereas the Shallow Offshore has single leg geothermal gradients pattern. In the two-leg dogleg geothermal pattern, a shallow interval of low geothermal gradient and a deeper interval of higher geothermal gradient are usually observed. The shallow interval of lower geothermal gradient is usually characterized by higher thermal conductivity whereas the deeper interval of higher geothermal gradients exhibits lower thermal conductivities. A sharp break occurs in the two gradient legs of the temperature ó depth profile. The shallow gradient belongs to the continental and/or continental transition (CT) sequence, whereas the deeper gradient belongs to the paralic/marine paralic sequence. The thickness of the lower geothermal gradient interval varies from 700m to 2000 m. The shape of the dogleg depends on the contrast in thermal gradient between the continental and the deeper paralic/marine paralic. If the contrast is low, the dogleg pattern appears close to a single leg model and a gentle curve replaces the kink. The single leg pattern occurs in the Shallow Offshore areas where high percentage interval (70 ó 80%) interval occurs at depths of 2900 ó 3600 m. In the Shallow Offshore, temperature profile or the geothermal gradient pattern show a uniform linear increase with depth.

The geothermal gradients pattern in the Eastern part of the Niger Delta is thus a reflection of the lithological variations in the area. The transition from one leg of the dogleg to another coincides with the change from the continental sandstones to the paralic / marine section. The temperature depth profiles used in calculating the thermal gradients are thus shown in figure 5.1 and in appendix 1. Geothermal gradient maps of the study area are shown in figures 5.2, 5.3 and 5.4.

5.1.1 Geothermal Gradients in the Shallow (Continental) section.

In the Central Swamp depobelt, the geothermal gradient in the continental sandstone is slightly above 10 $^{\circ}$ C/Km at the central part around Tabangh, Yomene and Mobazi fields. The geothermal gradients increase eastwards and westwards to

slightly above 18 °C/Km. In the Coastal Swamp depobelt, the geothermal gradient in the shallow / continental section varies between 10 °C/km ó 18 °C/Km in the western and central parts and increases eastwards to 26° C/Km (Fig. 5.2). In the Shallow Offshore, the geothermal gradient in the continental sandstones increases from about 14 °C/Km at the coastline to about 24 °C/Km in the J field. The geothermal gradient in the K field averages about 20°C/Km and increases eastwards to about 26 °C/Km. Geothermal gradients variation within the Shallow (Continental) section are summarized in table 5.1

5.1.2 Geothermal Gradients in the deeper (Marine / Paralic) section

In the deeper (marine/paralic) section, the geothermal gradient varies from between 18 $^{\circ}$ C/km to 30 $^{\circ}$ C/km in the west and central part of the Coastal Swamp and increases to 45 $^{\circ}$ C/Km at the eastern parts. (Fig.5.3). Northwards in the central parts of the Central Swamp, the geothermal gradients are slightly less than 20 $^{\circ}$ C/Km, but increases up to 45 $^{\circ}$ C/Km eastwards and westwards. The geothermal gradient in the marine/paralic section of the Shallow Offshore varies between 18 $^{\circ}$ 25 $^{\circ}$ C/Km in the eastern and central parts and increases eastwards towards the Qua-Ibo field. The geothermal gradients variation in the deeper (marine / paralic) section are summarized in table 5.2

5.1.3 Average Geothermal Gradient variation

In the Coastal Swamp, the average geothermal gradient varies between less than 12 $^{\circ}$ C/Km to 20 $^{\circ}$ C/Km in the western and central parts and increases eastwards up to 24 $^{\circ}$ C/Km towards the Qua Ibo field (Fig. 5.4). In the Central Swamp, the lowest values of average geothermal gradient of 14 $^{\circ}$ C/Km occur in the central parts around Tabangh, Mobazi and Yomene fields. The average geothermal gradient increases eastwards to 20 $^{\circ}$ C/Km and westwards to and 30 $^{\circ}$ C/Km. In the Central Swamp, the highest average thermal gradients of 23 $^{\circ}$ C/Km 30 $^{\circ}$ C/Km occur at Imo river-1 and Obigbo-1 wells. In the western part of the Shallow Offshore, the average thermal gradient varies between 14 $^{\circ}$ 24 $^{\circ}$ C/Km from the coastline to further offshore. It also increases eastwards to about 20 $^{\circ}$ C/Km in the K field and further eastwards to 26 $^{\circ}$ C/Km

| | | | Geothermal Gradient ^o C/Km | |
|----|------------------|-----------------|---------------------------------------|------|
| | Depobelt | Abbreviation | Low | High |
| 1 | Shallow Offshore | S _{HO} | 14 | 26 |
| 2 | Coastal Swamp | Cso | 10 | 26 |
| a. | Western part | Cso(a) | 10 | 18 |
| b. | Central part | Cso(b) | 10 | 18 |
| c. | Eastern part | Cso© | 10 | 24 |
| 3 | Central Swamp | Csw | 10 | 20 |

 Table 5.1: Summary of Geothermal Gradient variations for the Shallow Section (Continental Sandstones) across the depobelts in the study area

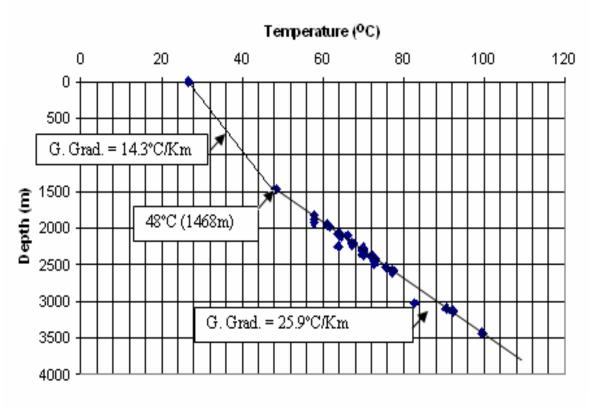


FIG. 5.1: Temperature-Depth plot for Bomu field

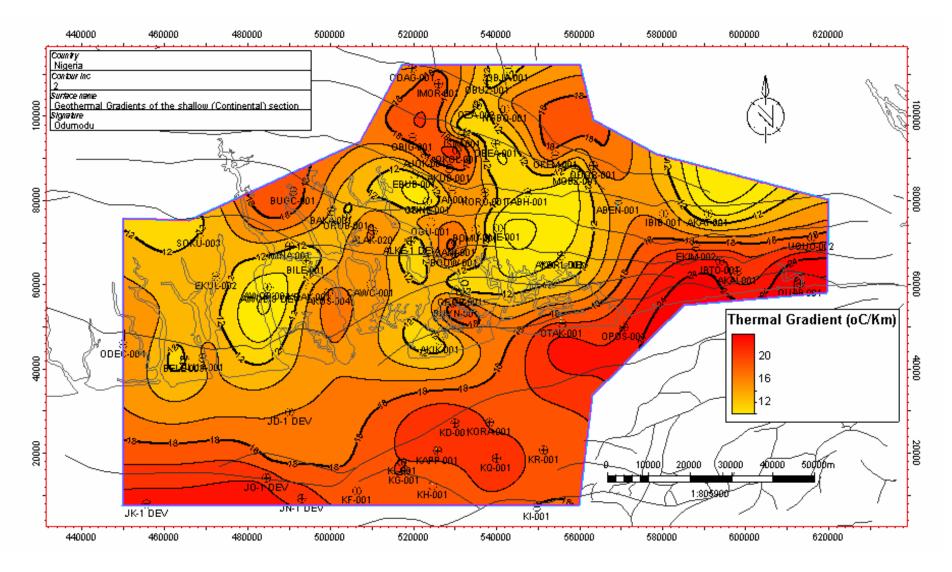
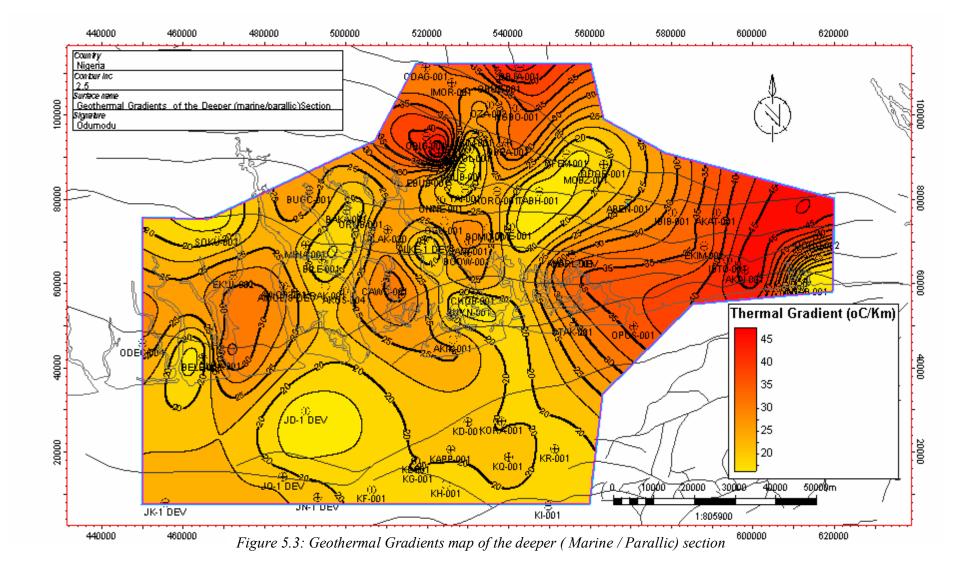


Figure 5.2 : Geothermal Gradients map of the Shallow (Continental) section



| | | | Geothermal Gradient ^o C/Km | |
|----|------------------|-------------------|---------------------------------------|------|
| | Depobelt | Abbreviation | Low | High |
| 1 | Shallow Offshore | \mathbf{S}_{HO} | 18 | 20 |
| 2 | Coastal Swamp | Cso | 20 | 45 |
| a. | Western part | Cso(a) | 18 | 30 |
| b. | Central part | Cso(b) | 20 | 30 |
| c. | Eastern part | Cso(c) | 30 | 45 |
| 3 | Central Swamp | Csw | 18 | 45 |

Table 5.2: Summary of Geothermal Gradient variations for the deeper (paralic/ marine section across the study area

| | Depobelt | Abbreviation | Geothermal Gradient °C/Km | |
|----|---------------------|-----------------|------------------------------|------|
| | | | Low | High |
| 1 | Shallow Offshore | S _{HO} | 14 | 26 |
| 2 | Coastal Swamp | Cso | 12 | 24 |
| a. | Western part | Cso(a) | 12 | 18 |
| b. | Central part | Cso(b) | 16 | 20 |
| c. | Eastern part | Cso(c) | 20 | 24 |
| 3 | Central Swamp | Csw | 14 | 32 |

Table 5.3: Summary of Average Geothermal Gradient values for the depobelts across the study area

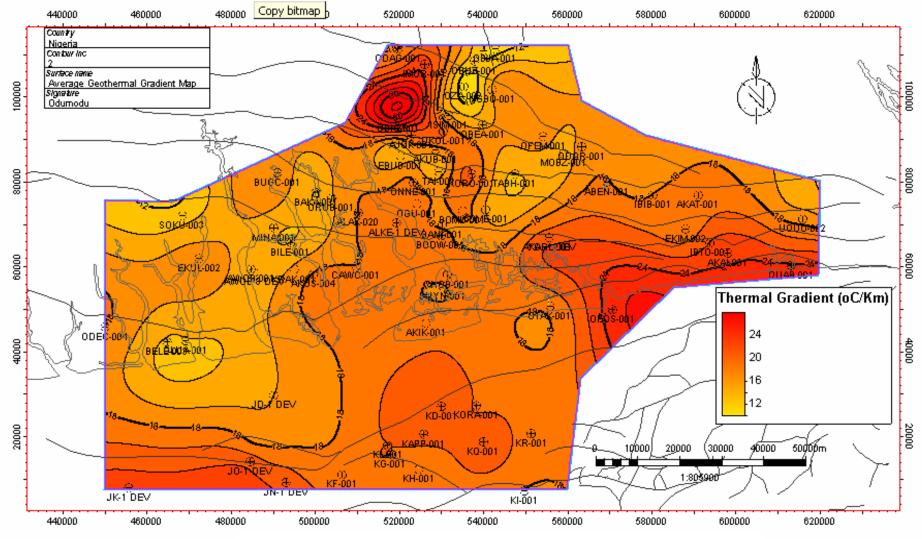


Figure 5.4: Average Geothermal Gradients map of parts of the Eastern Niger Delta

Least square fit to the combined reservoir and corrected bottom hole temperatures data gave the average geothermal gradient for the Central Swamp depobelt of the Niger as 19.3 ° C/km, with a correlation coefficient of about 0.66(Figure 5.5a). The temperature depth relationship in the Central Swamp depobelt can thus be predicted using the following equation:

$$T = 19.3z + 27 - \dots (29)$$

Where T is the surface temperature and z is the depth.

Least square fit to the combined reservoir and corrected bottom hole temperatures data gave the average geothermal gradient for the Coastal swamp depobelt of the Niger as 17.6 ° C/km, with a correlation coefficient of about 0.86. (Fig.5.5b)The temperature depth relationship in the Coastal Swamp depobelt can thus be predicted using the following equation:

T = 17.6z + 27 ------ (30)

Where T is the surface temperature and z is the depth.

Least square fit to the combined reservoir and corrected bottom hole temperatures data gave the average geothermal gradient for the Shallow Offshore depobelt of the Niger as 20.4° C/km, with a correlation coefficient of about 0.97. (Fig. 5.5c) The temperature depth relationship in the Coastal Swamp depobelt can thus be predicted using the following equation:

T = 20.4 z + 22 ------(31)

Where T is the surface temperature and z is the depth.

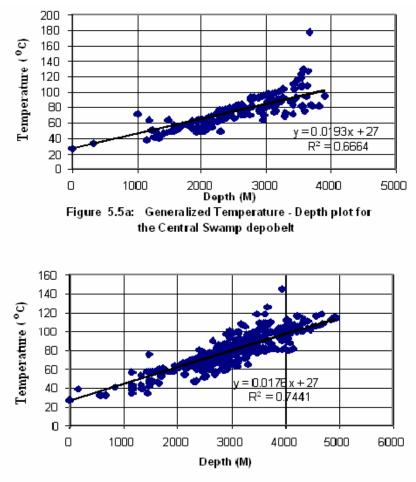
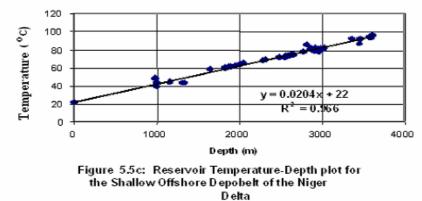


Figure 5.5b: Generalized Temperature - Depth plot for the Coastal Swamp Depobelt of the Niger Delta



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4.1 Subsurface Temperature Variations in the Niger Delta

The regional temperature fields in the Central Swamp, Coastal Swamp and Shallow Offshore depobelts of the Eastern Niger Delta were characterized using data collected from reservoir temperature and corrected bottom-hole temperatures. The estimated temperatures are presented in temperature maps showing the temperature fields at specific depths of 1000m, 2000m, and 3000m. (Fig. 5.6a-c and Fig. 5.7a-c) Mapping the depth to isotherms of 100°C and 150 °C (i.e. isothermal maps) (Fig. 5.9a and 5.9b) were also utilized in this study to evaluate the temperature-depth relationships of the Eastern Niger Delta. The observed temperature anomalies may be largely attributed to the variations in the thermal conductivity of the sediments, thickness of the formations, net gross or lithological control and depth to the top of the basement. The variable sediment accumulation in the area has resulted in differences in the overall thermal conductivity of the sediment and the temperature fields reflect such differences. The temperature field is also influenced by gross lithological changes or sedimentation rate. Regions of low thermal anomalies correspond with areas of high sand percentage. It is a very well known fact that sands are better conductors than shale and will therefore show lower thermal anomalies. The thickness of the sandy intervals of the Benin and Agbada formations is another factor that influences thermal anomalies in this part of the Niger delta. Minimum temperatures coincide with areas of maximum thickness of the sandy Agbada and Benin formations. This suggests a cooling effect of the continental sands. The convection currents set up in the freely moving groundwater helps in lowering the temperature as well as the cooling effect due to conduction.

5.3 Temperature fields

The temperature fields at three depth levels of 1000m, 2000m, and 3000m were evaluated to understand the variable temperature pattern of the Niger Delta. The average geothermal gradient and variable geothermal gradient models were utilized in computing the temperatures at the three depth intervals. The results of this analysis are shown in tables 5.4, 5.5 and figures.5.6 a-c, 5.7 a-c and Fig 5.8 a-e. The temperatures estimates from the average geothermal gradient model are quite higher than that of the variable geothermal gradient model. Since the average geothermal gradient model overestimates temperatures, the variable geothermal gradient model was used to describe the variations in temperature fields.

5.3.1 Temperature Fields at Depth of 1000m (3048ft)

At shallow depths 1000m (3048ft) (Fig. 5.6a), depressed temperatures of about 39 ó 45 ° C were observed in the western and central part of the Eastern Coastal Swamp. The temperatures become elevated to higher values ranging from 45° C ó 52° C in the eastern parts of the Coastal Swamp and up to 56° C, northwards in the Central Swamp. Depressed temperatures observed in the western part of the study area, which corresponds to the central part of the Niger Delta, is influenced by the great thickness of sands and great depths to the basement. Convection currents set up by the free movement of groundwater in the continental sandstones also help in lowering the heat being conducted to the surface. The shallow depth to basement, shaliness and closeness to the Cameroun volcanic line could influence the elevated temperatures in the eastern part.

5.3.2 Temperature Fields at Depth of 2000m (6048ft)

At depths of about 2000m (6048 ft) (Fig. 5.6b), depressed temperatures (<55 $^{\circ}$ C) are observed in the western part of the study area. Moderate temperatures ranging from 55 to 65 $^{\circ}$ C are observed in the central part of the Coastal Swamp. Temperature variations in this area are clearly influenced by lithologic differences. Anomalously high temperatures ranging from 65 to 75 $^{\circ}$ C are also observed in the eastern part of the Coastal Swamp and in the Central Swamp depobelt in the north. The higher temperature in the north-western part of the study area (i.e. the Central Swamp) is likely to be influenced by hydrothermal convection of fluids coming up from the underlying over pressured Akata Formation.

5.3.3 Temperature Field at Depth of 3000m (9096ft)

At depths of about 3000m (9096ft) (Fig. 5.6c), the temperature field maintain the same pattern as in shallower interval, but with minor changes. Lower temperatures (70 ó 75 $^{\circ}$ C) are observed in the western part of the Eastern Coastal Swamp. Moderate temperatures ranging from 75 to 85 $^{\circ}$ C were observed in the central part of the Coastal Swamp. Generally in the Coastal Swamp temperatures become elevated to about 85 -100 $^{\circ}$ C in the eastern parts as well as north-westwards in the Central Swamp. The higher temperatures are greatly influenced by lithology.

| | Depobelt | Temperature field at 1000m (3048ft) (°C) | <i>Temperature</i> <i>field at 1000m</i> <i>(6096ft) (°C)</i> | Temperature field at 1000m (9144ft) (°C) |
|----|------------------|--|---|--|
| 1 | Shallow Offshore | 41 ó 45 | 59 ó 65 | 78 ó 86 |
| 2 | Coastal Swamp | 39 ó 52 | 45 ó 76 | 62 ó 105 |
| a. | Western part | 39 ó 42 | 45 ó 55 | 62 ó 75 |
| b. | Central part | 41 ó 45 | 55 ó 65 | 75 ó 85 |
| c. | Eastern part | 45 ó 52 | 65 ó 75 | 85 ó 105 |
| 3 | Central Swamp | 39 - 50 | 52 - 72 | 70 - 105 |

Table 5.4: Temperature fields (Variable Geothermal Gradient model)

Table 5.5: Temperature fields (Average or Constant Geothermal Gradient model)

| | Depobelt | Temperature field at 1000m (3048ft) (°C) | Temperature field at 2000m (6096ft) (°C) | Temperature field at 3000m (9144ft) (°C) |
|----|------------------|--|--|--|
| 1 | Shallow Offshore | 40 ó 50 | 55 ó 80 | 70 ó 100 |
| 2 | Coastal Swamp | 40 ó 50 | 50 ó 75 | 63ó 100 |
| a. | Western part | 40ó 45 | 50ó 60 | 63 ó 75 |
| b. | Central part | 40 ó 48 | 60 ó 65 | 75 ó 85 |
| c. | Eastern part | 47 ó 50 | 65 ó 75 | 85 ó 100 |
| 3 | Central Swamp | 40 - 58 | 50 - 90 | 70 - 105 |

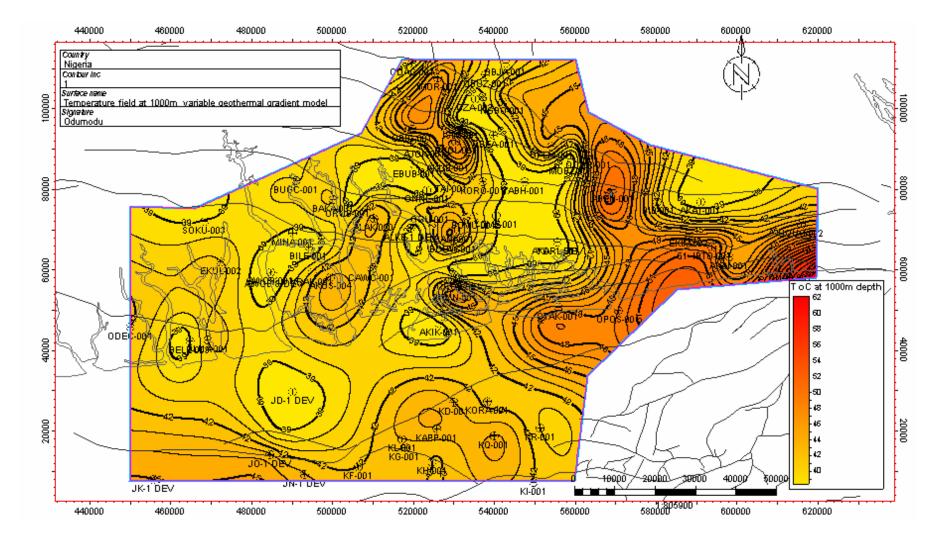


Figure 5.6a : Temperature field at 1000m (Variable Geothermal Gradient model)

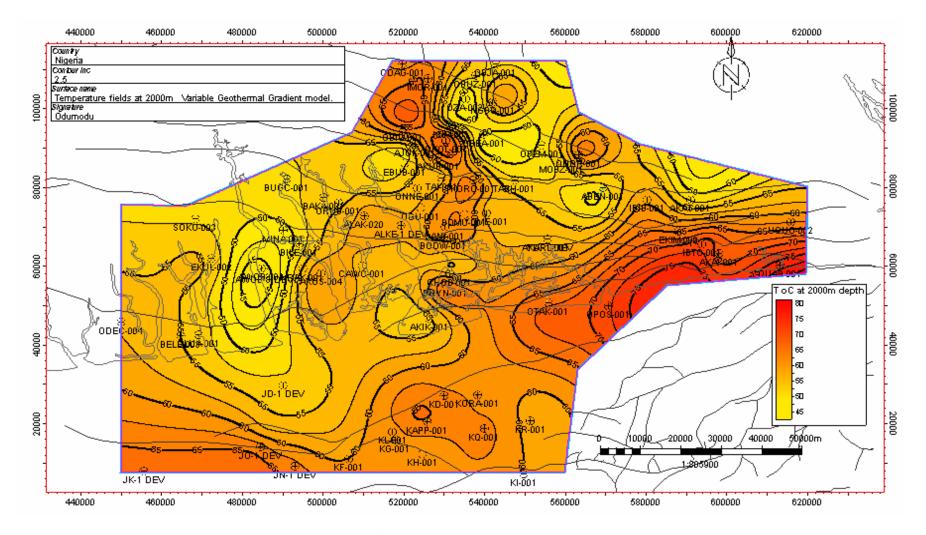


Figure 5.6b : Temperature field at 2000m (Variable Geothermal Gradient model)

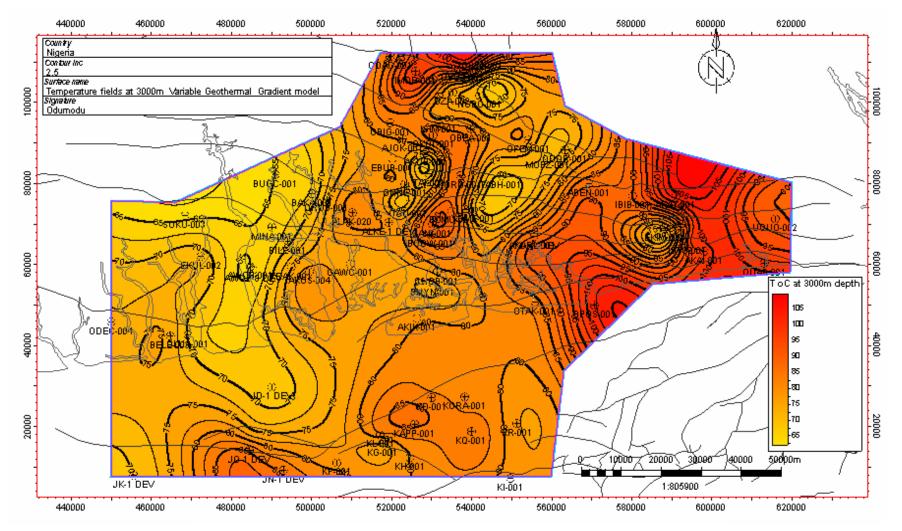


Figure 5.6c : Temperature field at 3000m (Variable Geothermal Gradient model)

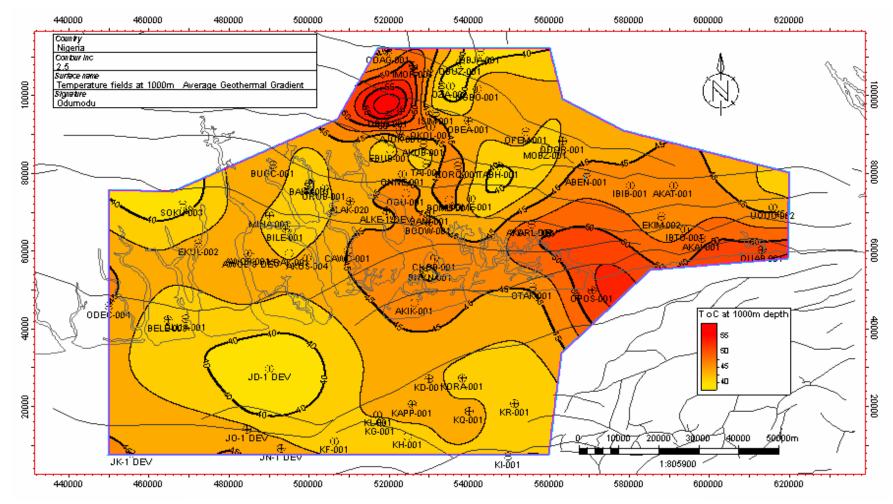


Figure 5.7a : Temperature field at 1000m (Average Geothermal Gradient model)

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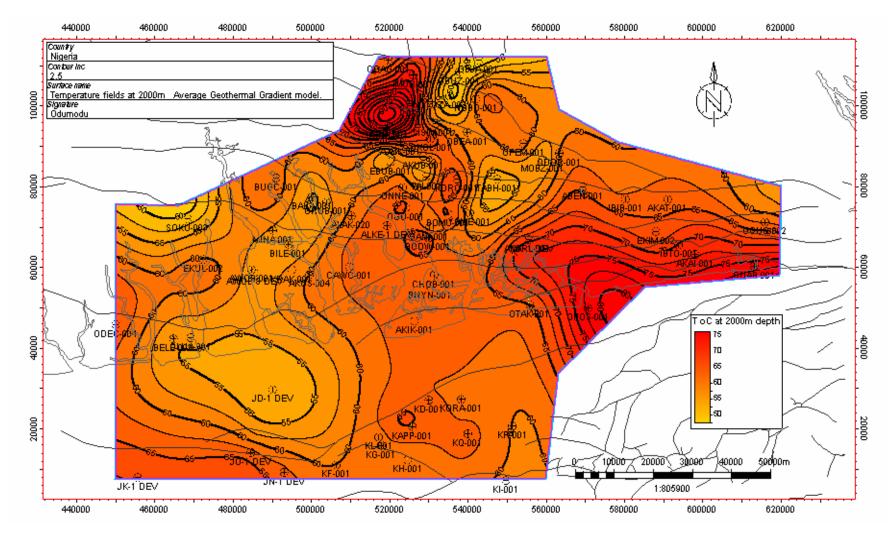


Figure 5.7b : Temperature fields at 2000m (Average Geothermal Gradient model)

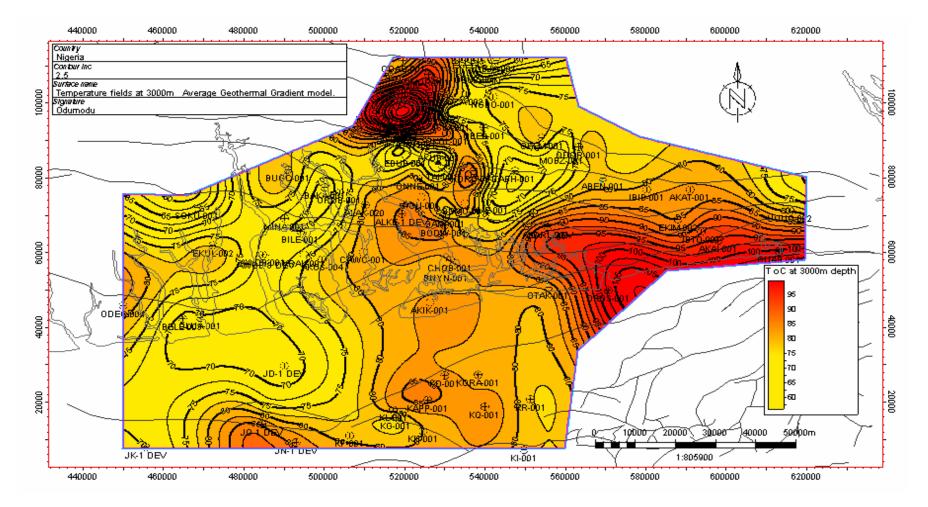


Figure 5.7c : Temperature field at 3000m (Average Geothermal Gradient model

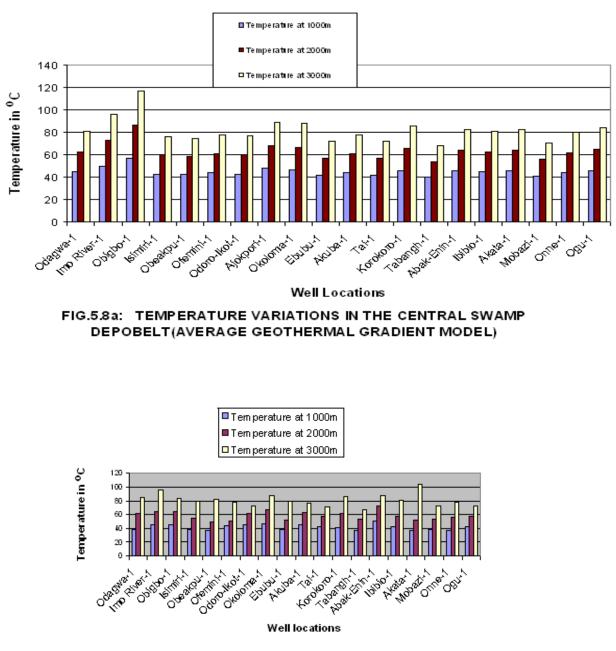
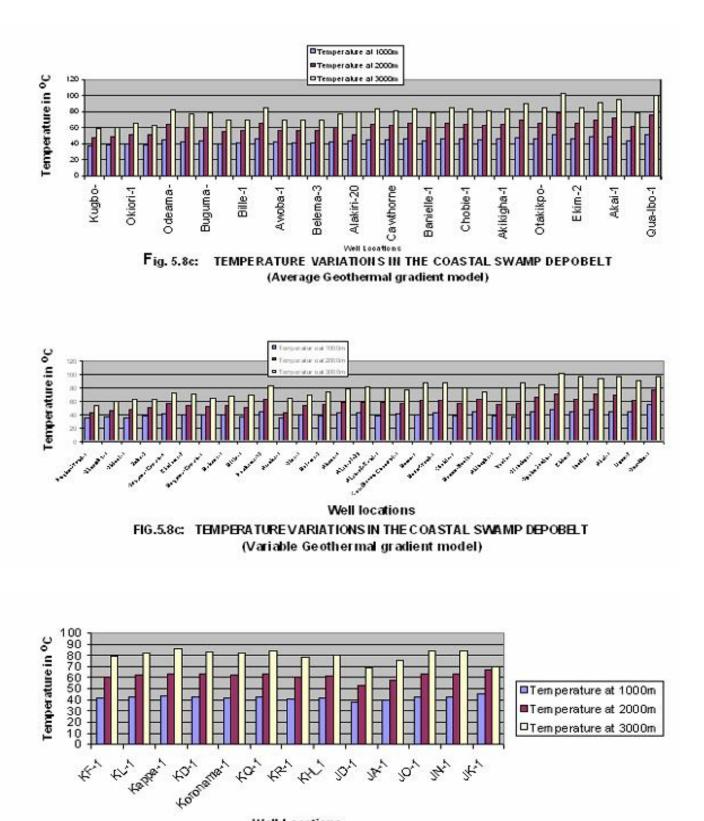


FIG. 5.8b: TEMPERATURE VARIATIONS IN THE CENTRAL SWAMP DEPOBELT (Variable Geothermal Gradient model)



Well Locations

FIG. 5.8e. TEMPERATURE VARIATIONS IN THE SHALLOW OFFSHORE DEPOBELT (Average Geothermal Gradient Model)

5.3.4 Isothermal Maps

Temperature distributions in the study area were also evaluated using 100°C and 150°C isothermal maps (Figures 5.9a and 5.9b, Table 5.6 and 5.7) One remarkable aspect of this mapping is that these isotherms are shallower in areas having higher thermal gradients and deeper in areas with lower thermal gradients. The depths to 100°C isotherm ranges from 4000m to 5000m in the western parts of the Eastern Coastal Swamp. It decreases eastwards from about 4000m to 2800m in the Coastal Swamp. In the central parts of the Coastal Swamp, the depth ranges from 4000m to 5000m, but decreases eastwards and westwards to less than 3000m. In the Shallow Offshore, the depth ranges from 3500 $\acute{0}$ 4000m. The depth to 150 $^{\circ}$ C isotherms shows a similar pattern to the 100 ° C isotherm. The shallowest depths to 150°C isotherm occur in the east (4500-5,000m) and in the northwest (4500-5,000m). Greater depths to 150 ° C occur in the west (6,000m- 9000m), in the central parts of the Central Swamp (6,000-9,000 m) and in the south (coastal area) (6,000m ó 9,000m). These isotherms are close to the temperatures of 116 $^{\circ}$ C (240 $^{\circ}$ F) and 150 °C (300 °F) which Evamy et al (1978) considered to represent the top of the oil and gas windows for Tertiary provinces.

| | | | Depth Range to 100° C isotherm (m) | |
|----|------------------|------------------|---|------|
| | Depobelts | Abbreviatio n | Low | High |
| 1 | Shallow Offshore | S _{HO} | 3645 | 4084 |
| 2 | Coastal Swamp | Cso | 2933 | 5369 |
| a. | Western part | Cso(a) | 3780 | 5369 |
| b. | Central part | Cso(b) | 3431 | 5078 |
| c. | Eastern part | Cso© | 2933 | 3305 |
| 3 | Central Swamp | Csw | 3113 | 5313 |

Table 5.6: Isothermal depths at $100^{\circ}C(212^{\circ}F)$

Table 5.7: Isothermal depths at $150^{\circ}C(300^{\circ}F)$

| | Depobelts | Abbreviation | Depth Range to 150 °C isotherm (| |
|----|------------------|-------------------|----------------------------------|------|
| | | | Low | High |
| 1 | Shallow Offshore | \mathbf{S}_{HO} | 5981 | 6809 |
| 2 | Coastal Swamp | Cso | 4314 | 9280 |
| a. | Western part | Cso(a) | 5612 | 8680 |
| b. | Central part | Cso(b) | 5026 | 9280 |
| c. | Eastern part | Cso© | 4314 | 4867 |
| 3 | Central Swamp | Csw | 4221 | 6693 |

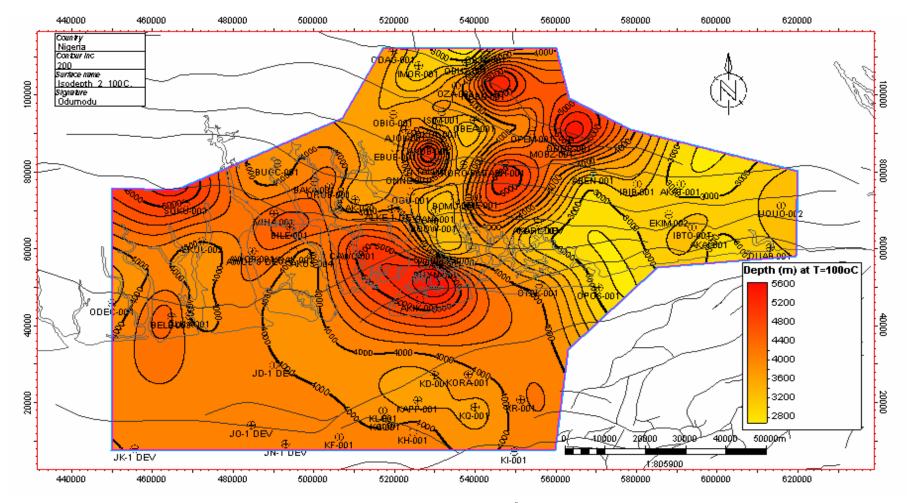


Figure 5.9a: Isothermal depths at 100°C.

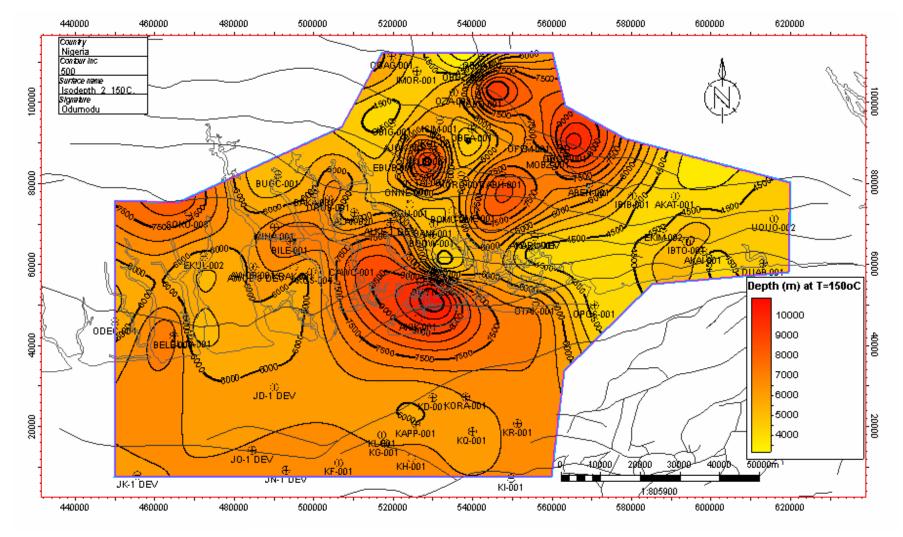


Figure 5.9b: Isothermal denths at 150°C.

5.4 Sand Percentage Distribution in the Niger Delta.

In a vertical section, the sand distribution in the Niger delta consists of 100 ó 70 % for the Benin Formation, 70 ó 30 % for the Agbada Formation to less than 30% for the Akata Formation (Fig. 5.10) This therefore suggests that sand percentages in the Niger delta decreases with depth. The sand percentage map for the depth interval of 0 ó 1312m (Fig. 5.11) also suggests that highest sand percentages of about 95% occur in the centre of the delta around Soku, Ekulama, Awoba and Buguma Creek fields. It all shows that the sand percentage decreases from this part of the Coastal Swamp from a value of 95% to the offshore area to a value of about 75%. It also shows that sand percentages decreases from the western part of the eastern Coastal Swamp, at a value of 95% to the Central Swamp and eastwards at a value of about 80%. Figure 5.11 represents continental deposition that is usually characterized by sand percentages that is greater than 80%. For the depth interval of 1312 ó 3000m (Fig. 5.12), highest sand percentages of about 80% occur at the centre of the delta around Soku, Ekulama, and Awoba and Buguma Creek fields. At this depth interval, sand percentages decreases offshore and eastwards to about 50% and 20% respectively. The sand percentages map generally has an alternating high and low sand percentages distribution in the Niger delta. Pockets of high and low sand percentages occur respectively within low and high sand percentages regions. These maps may therefore indicate a regional trend in the depositional pattern of the delta.

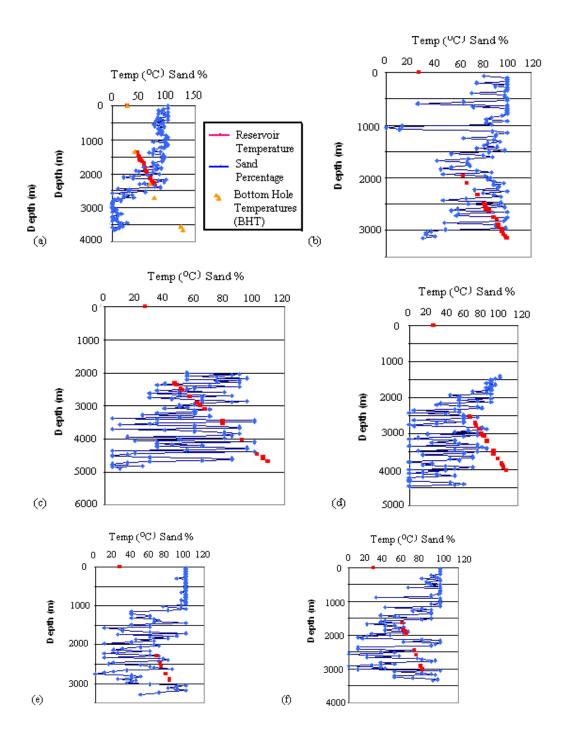


Figure 5.10: Plots of Temperature and Sand Percentage against depth for some wells (a) Akata -1 (Central Swamp) (b) Imo River-1 (Central Swamp) (c) Awoba -1 (Coastal Swamp (d) Odeama Creek -1 (Coastal Swamp) (e) KD-1 (Shallow Offshore (f) KL-1 (Shallow Offshore

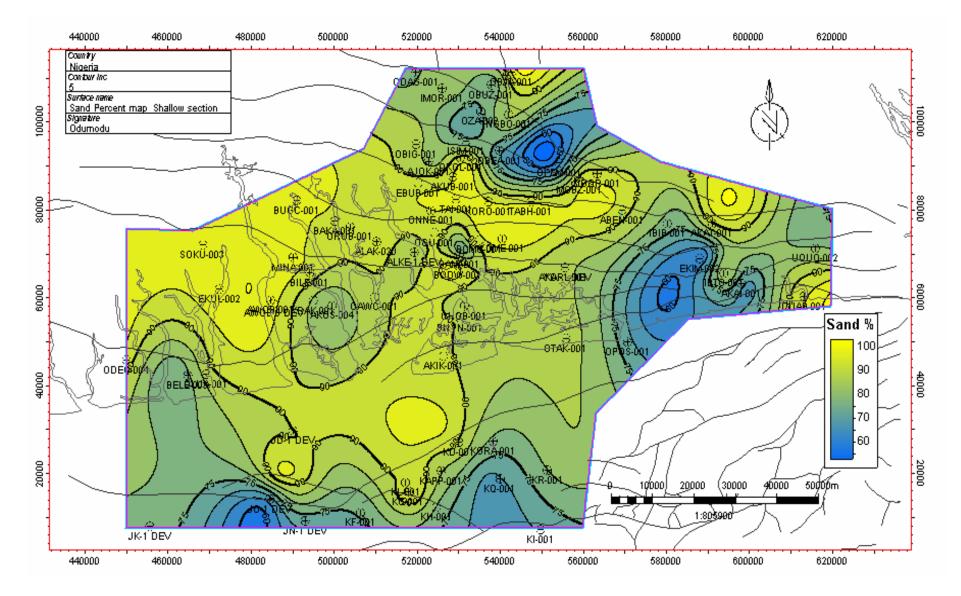


Figure 5.11a: Sand Percentage map for the shallow (Continental section)

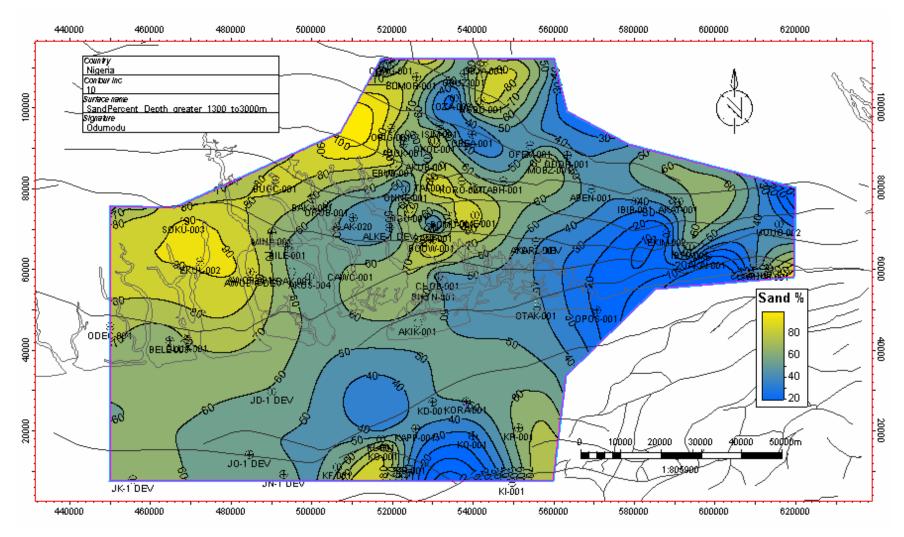


Figure 5.11b: Sand Percentage map for the deeper (Marine / Parallic section)

5.5 Heat Flow variations in the Niger Delta

Heat flow values were computed for seventy (70) wells in the Central Swamp, Coastal Swamp and the Shallow Offshore depobelts by calibrating temperatures predicted using the rifting model with observed temperatures using Petromod 1-D modelling software. The computed heat flow ranges from 29 mWm⁻² - 55 mWm⁻², and an average of 42.5 mWm⁻² (Fig. 5.12). This represents a heat flow unit (HFU) of 0.69 ó 1.31 and an average of about 1.00 HFU. Higher heat flow values (45 ó 55 mWm⁻²) were observed in the western parts of the Central Swamp as well as in the eastern parts of Central Swamp, the Coastal Swamp and the Shallow Offshore. Lower heat flow values (< 35 mWm⁻²) were observed in the coastal Swamp and the Shallow Offshore.

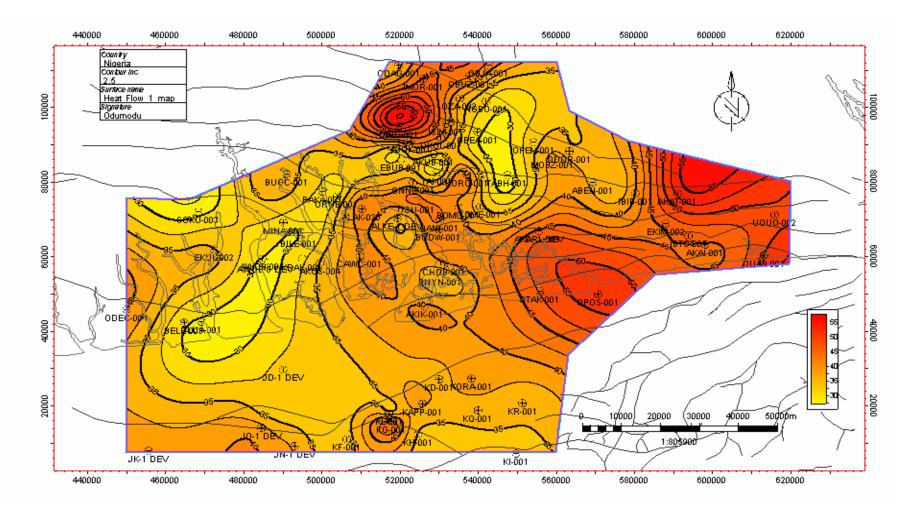


Figure 5.12: Heat Flow Map of parts of the Eastern Niger Delta

Burial History and Hydrocarbon Maturation Modelling

5.6

The wells for which burial history and hydrocarbon maturation modelling include four wells, namely Obigbo ó 1, Opobo-South-4, Akaso-4 and Kappa ó 1. The wells were chosen to represent different depositional, structural and thermal settings Obigbo-1 is located within the Central Swamp depobelt. Opobo-South-4 and Akaso-4 are located in the Coastal Swamp while Kappa-1 is in the Shallow Offshore. The four wells were modelled to reconstruct their hydrocarbon generative histories. Predicted maturation and timing of hydrocarbon generation are based on Easy%R_o of Sweeney and Burnham (1990), while the calculation of kerogen transformation is based on the kinetic dataset of Burnham (1989) for type II/III kerogen. Maturation stages and their corresponding vitrinite reflectance values are illustrated in table 5.8.

| Table 5.8: | Thermal Maturity stages(Sweeney |
|--------------|---------------------------------|
| and Burnham, | 1989). |

| Maturity stage | Vitrinite Reflectance (R ₀ %) |
|---------------------|--|
| Immature | < 0.6 % |
| Early Mature | 0.6 - 0.7 % |
| Mid Mature | 0.7 - 1.0 % |
| Late Mature | 1.0 - 1.3 % |
| Main gas generation | 1.3 ó 2.2 % |

5.6.1 Thermal Modelling of Obigbo – 1 well (Central Swamp)

The input data used for the modelling is given in table 5.9. The well was drilled to a depth of 3734m, in Lower Miocene sediments. The well did not penetrate into the Oligocene, Eocene, and Palaeocene sediments. The thickness of the Oligocene, Eocene and Palaeocene sediments were considered to be the same as encountered at Midim -1 well, which is a nearby well. (Table 4.3).

Maturation was modelled using Petromod 1-D modelling software with vitrinite relectance being calculated using Easy% R_o of Sweeney and Burnham (1990). The predicted vitrinite reflectance values cannot be compared with measured values because no vitrinite reflectance data exists for the well. However, the maturity data were established by calibrating calculated temperature against the measured temperature data for the well. A good fit between calculated and measured temperature data was achieved by using the rifting ó subsidence thermal model, whereby a high heat flow value of 90 mWm⁻² is applied at 85 Ma, being the break-up phase of the basins initiation.

Burial history diagrams showing isotherms and maturity windows for Obigbo-1 well are shown in figure 5.13. In this study, Upper Miocene, Lower Miocene Oligocene, Eocene and Palaeocene sediments are considered as effective source rocks. The modelling suggests that the Upper Miocene and upper parts of the Lower Miocene (Ro < 0.6%) are immature for oil generation. The modelling also suggests that the basal parts of the Lower Miocene are in the early mature zone (0.60% - 0.70%). The modelling shows that the upper parts of the Oligocene are in the mid-mature zone (0.70 \pm 1.0% Ro) while the middle parts of the Oligocene are in the late mature (1.0% - 1.3%) stage of oil generation. This study also suggests that the Lower Oligocene, the Eocene and the Palaeocene are in the gas generation

phase (Ro = 1.3 \circ 2.2). A heat flow of 53 mWm⁻² is calculated from BHT temperatures with a surface temperature of 27° C.

| | т | ABLI | E 5.9 : | MAIN I | NPUT FC | R OBI | GBO - 1 | WELL | (CEN | TRAL SV | VAMI | P) | |
|-------------|------|------|---------|--------|----------|---------|----------|---------|--------|-----------|------|------------|---------|
| | Тор | Base | Thick | Eroded | Depo | Depo | Eroded | Eroded | Lithol | | TOC | | H(mgHC/ |
| Layer | (m) | (m) | ness(m) | (m) | from(Ma) | to (Ma) | from(Ma) | to (Ma) | ogy | PSE | % | Kinetic | gTOC |
| Pliocene | | | | | | | | | SAND | Over | | | |
| -Recent | 0 | 591 | 591 | | 3 | 0 | | | shaly | burden | | | |
| U.Miocene | | | | | | | | | SAND | | | | |
| (P780/P770) | 591 | 1447 | 856 | | 9.5 | 6.5 | | | shaly | Sealrock | | | |
| | | | | | | | | | SHAL | Reservoir | | | |
| M.Miocene | 1447 | 2559 | 1112 | | 16 | 116 | | | Eshaly | rock | | | |
| | | | | | | | | | SAND | | | | |
| | | | | | | | | | &SHA | Source | | Burnham | |
| L.Miocene | 2559 | 3734 | 1175 | | 19 | 15.5 | | | LE | rock | 1.4 | (1989) II | 100 |
| | | | | | | | | | SHAL | Source | | Burnham | |
| Oligocene | 3734 | 5479 | 1745 | | 35 | 26.2 | | | E | rock | 1.8 | (1989) III | 150 |
| | | | | | | | | | SHAL | Source | | Burnham | |
| Eocene | 5479 | 5635 | 156 | | 57 | 35.4 | | | Esand | rock | 2.2 | (1989) II | 200 |
| | | | | | | | | | SHAL | Source | | Burnham | |
| Paleocene | 5635 | 5976 | 341 | | 66 | 56.5 | | | Esilt | rock | 2.4 | (1989) III | 250 |
| | | | | | | 65.5 | | | | | | | |

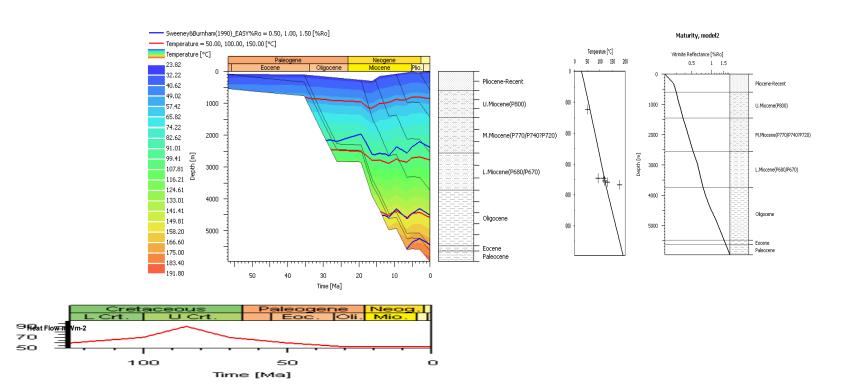


Fig. 5.13: Burial History chart showing isotherms, organic maturity and model calibration with temperature data for Obigbo. 1 well in the Central Swamp depoblet of the Niger Delta.

5.6.2 Thermal modelling of Akaso – 4 well (Coastal Swamp)

Input data used in the modelling is given in table 5.10. The wells were drilled to a depth of 4306.4m, in Middle Miocene sediments. The well did not penetrate into the Oligocene, Eocene, and Palaeocene sediments. The wells were extrapolated to the base of the Palaeocene, using the thickness of these units as evaluated from seismic sections in the vicinity of the well(Personal communication with Frielingsdorf) (Table 4.4). Maturation was modelled using Petromod 1-D modelling software with vitrinite being calculated using Easy% R_o of Sweeney and Burnham (1990). The predicted vitrinite reflectance values cannot be compared with measured values because no vitrinite reflectance data exists for the well. However, the maturity data were established by calibrating calculated temperature against the measured temperature data for the well. A good fit between calculated and measured temperature data was achieved by using the rifting ó subsidence thermal model, whereby a high heat flow value of 90 mWm⁻² is applied at 85 Ma, being the break-up phase of the basins initiation.

Burial history diagrams showing isotherms and maturity windows for Akaso-4 are shown in figure 5.14. In this study, the Miocene, Oligocene, Eocene and Palaeocene sediments are considered as effective source rocks. The modelling suggests that the Miocene rocks (Ro < 0.6%) are immature for oil generation. The predicted maturity for the Oligocene, Eocene and Palaeocene rocks ranges from 0.60 % to 1.1 %, which indicates that these source rocks are mature for oil generation. A heat flow of 35 mWm⁻² is calculated from PRT temperatures with a surface temperature of 27° C.

| | TABLE 5.10 : MAIN INPUT FOR AKAS0 - 4 WELL (COASTAL SWAMP) | | | | | | | | | | | | | |
|--------------------------|--|-------------|------------------|---------------|----------------------|------|--------------------|-------------------|----------------|-------------------|----------|-----------------------|----------------------|--|
| Layer | Top (m) | Base (m) | Thick ness(m) | Eroded (m) | Depo from(Ma) | | Eroded from(Ma) | Eroded to (Ma) | Litho logy | PSE | тос % | Kinetic | HI (mgHC /gTOC | |
| Pliocene -Recent | 0 | 2315 | 2315 | | 5.6 | 0 | | | SAND shaly | Over burden | | | | |
| U.Miocene (P780/P770) | 2315 | 2858 | 543 | | 9.5 | 5.6 | | | SAND& SHALE | Sealrock | | | | |
| M.Miocene | 2858 | 4304 | 1446 | | 12.1 | 9.5 | | | sand | Reservoir rock | | | | |
| L.Miocene | 4304 | 4719 | 415 | | 17.7 | 12.1 | | | SHALE sand | Source rock | 1.2 | Burnham (1989) II | 100 | |
| Oligocene | 4719 | 5355 | 536 | | 35.4 | 23.3 | | | SHALE | Source rock | 1.4 | Burnham (1989) III | | |
| U. Eocene | 5255 | 5955 | 700 | | 40.4 | 35.4 | | | SHALE sand | Source rock | 1.6 | Burnham (1989) II | | |
| L. Eocene | 5955 | 6655 | 700 | | 56.7 | 40.4 | | | SHALE sand | Source rock | 2 | Burnham (1989) III | | |
| Paleocene | 6655 | 7355 | 700 | | 65.5 | 56.7 | | | SHALE silt | Source rock | 2.3 | Burnham (1989) II | | |
| | | | | | | 65.5 | | | | | | | | |

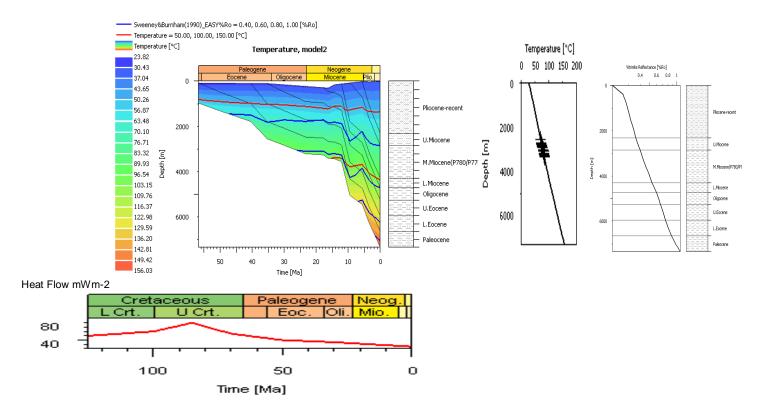


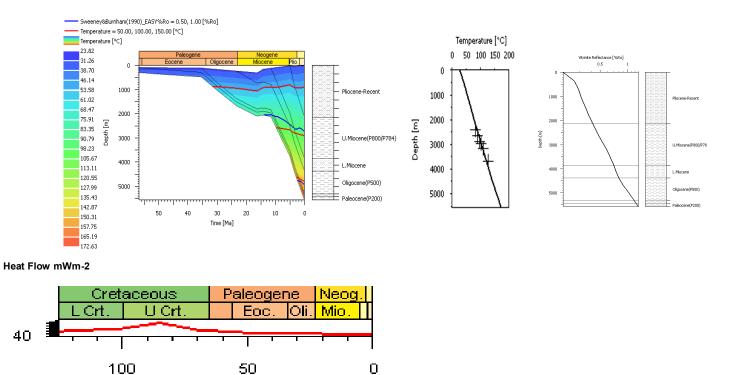
Fig. 5.14: Burial History chart showing isotherms, organic maturity and model calibration with temperature data for Akaso 4 well in the Coastal Swamp depobelt of the Niger Delta.

5.6.3 Thermal Modelling of Opobo South – 4 well

The input data used for the modelling is given in table 5.11. The well was drilled to a depth of 3878.3m, in Lower Miocene sediments. The well did not penetrate into the Oligocene, Eocene, and Palaeocene sediments. The thicknesses of the Oligocene, Eocene and Paleocene sediments were considered to be the same as encountered at Nsit-1 well, which is a nearby well. (Table 4.4). Maturation was modelled using Petromod 1-D modelling software with vitrinite being calculated using Easy% R_o of Sweeney and Burnham (1990). The predicted vitrinite reflectance values cannot be compared with measured values because no vitrinite reflectance data exists for the well. However, the maturity data were established by calibrating calculated temperature against the measured temperature data for the well. A good fit between calculated and measured temperature data was achieved by using the rifting ó subsidence thermal model, whereby a high heat flow value of 90 mWm⁻² is applied at 85 Ma, being the break-up phase of the basins initiation.

Burial history diagrams showing isotherms and maturity windows for Opobo South - 4 are shown in figure 5.15. In this study, Upper Miocene, Lower Miocene Oligocene, Eocene and Palaeocene sediments are considered as effective source rocks. The modelling suggests that the upper parts of the Upper Miocene (Ro < 0.6%) are immature for oil generation. The modelling also suggests that the basal part of the Upper Miocene is within the early mature zone (0.60% - 0.70%), while the Lower Miocene and the upper part of the Oligocene are in the mid-mature zone (0.70% - 1.0%). The modelling shows that the lower part of the Oligocene, the Eocene and the Palaeocene are in the late mature (1.0% - 1.3%) stage of oil generation. A heat flow of 51 mWm⁻² is calculated from PRT temperatures with a surface temperature of 27° C.

| | TABLE 5.11 : MAIN INPUT FOR OPOBO SOUTH - 4 WELL (COASTAL SWAMP) | | | | | | | | | | | | |
|-------------|--|-------|---------|--------|----------|---------|----------|---------|-------|------------|-----|------------|---------|
| | Тор | Base(| Thick | Eroded | Depo | Depo to | Eroded | Eroded | Litho | | тос | | HI(mg |
| Layer | (m) | m) | ness(m) | (m) | from(Ma) | (Ma) | from(Ma) | to (Ma) | logy | PSE | % | Kinetic | HC/gTOC |
| Pliocene | | | | | | | | | SAND | | | | |
| -Recent | 0 | 2139 | 2139 | | 5 | 0 | | | shaly | Overburden | | | |
| U.Miocene | | | | | | | | | SHALE | | | | |
| (P800/P784) | 2139 | 3865 | 1726 | | 11.5 | 5 | | | sand | Sealrock | | | |
| | | | | | | | | | SHALE | Reservoir | | Burnham | |
| L.Miocene | 3865 | 4370 | 505 | | 23.3 | 11.5 | | | &SAND | rock | 1.2 | (1989) II | 100 |
| Oligocene | | | | | | | | | | Source | | Burnham | |
| (P500) | 4370 | 5309 | 939 | | 35.4 | 23.3 | | | SHALE | rock | 1.6 | (1989) III | 150 |
| Eocene | | | | | | | | | SHALE | Source | | Burnham | |
| (P370/P330) | 5309 | 5429 | 120 | | 56.7 | 35.4 | | | sand | rock | 2 | (1989) III | 250 |
| Paleocene | | | | | | | | | SHALE | Source | | Burnham | |
| (P200) | 5429 | 5575 | 146 | | 65.5 | 56.7 | | | silt | rock | 2.4 | (1989) III | 300 |
| | | | | | | 65.5 | | | | | | | |



Time [Ma]

Fig. 5.15: Burial History chart showing isotherms, organic maturity and model calibration with temperature data for Opobo South - 4 well in the Coastal Swamp depobelt of the Niger Delta.

5.6.4 Thermal Modelling of Kappa – 1 well (Shallow Offshore)

Input data used in the modelling is summarized in table 5.12. The well was drilled to a depth of 3622.7m, in Middle Miocene sediments. The well did not penetrate into the Oligocene, Eocene, and Palaeocene sediments. The wells were extrapolated to the base of the Palaeocene, using the thickness of these units as evaluated from a nearby offshore well (Uge ST-1) (Table 4.3). Maturation was modelled using Petromod 1-D modelling software with vitrinite being calculated using Easy% R_o of Sweeney and Burnham (1990). The predicted vitrinite reflectance values cannot be compared with measured values because no vitrinite reflectance data exists for the well. However, the maturity data were established by calibrating calculated temperature against the measured temperature data for the well. A good fit between calculated and measured temperature data was achieved by using the rifting δ subsidence thermal model, whereby a high heat flow value of 90 mWm⁻² is applied at 85 Ma, being the break-up phase of the basins initiation.

Burial history diagrams showing isotherms, organic maturity and temperature calibration for Kappa -1 well are shown in figure 5.16. In this study, the Upper Miocene, Lower Miocene, Oligocene, Eocene and Palaeocene sediments are considered as effective source rocks. The modelling suggests that the Upper Miocene, the Lower Miocene and the Upper Oligocene are immature (Ro < 0.6%) source rocks. The modelling also suggests that basal part of the Oligocene, the Eocene and the Palaeocene are within the early to mid-mature stages (0.60 % to 1.0 %) of oil generation. A heat flow of 38 mWm⁻² is calculated from PRT temperatures with a surface temperature of 22° C.

115

| | Тор | Base | Thick | Eroded | Depo | Depo | | Eroded | Litho | | тос | | HI(mgH |
|-------------|------|------|---------|--------|----------|---------|----------|---------|-------|-----------|-----|------------|--------|
| Layer | (m) | (m) | ness(m) | (m) | from(Ma) | to (Ma) | from(Ma) | to (Ma) | logy | PSE | % | Kinetic | C/gTOC |
| U. Pliocene | | | | | | | | | | Over | | | |
| -Recent | 0 | 567 | 567 | | 3 | 0 | | | SAND | burden | | | |
| L.Pliocene | | | | | | | | | SAND | Seal | | | |
| (P880/P870) | 567 | 1027 | 460 | | 5 | 3 | | | shaly | rock | | | |
| | | | | | | | | | SAND | | | | |
| U.Miocene | | | | | | | | | & | Reservoir | | | |
| (P860/P840) | 1027 | 3606 | 2579 | | 6.7 | 5 | | | SHALE | rock | | | |
| | | | | | | | | | SAND | | | | |
| | | | | | | | | | &SHAL | Source | | Burnham | |
| L.Miocene | 3606 | 4021 | 415 | | 23 | 16.3 | | | E | rock | 1.6 | (1989) II | 100 |
| | | | | | | | | | | Source | | Burnham | |
| Oligocene | 4021 | 4831 | 810 | | 35 | 23.3 | | | SHALE | rock | 1.8 | (1989) III | 150 |
| | | | | | | | | | SHALE | Source | | Burnham | |
| Eocene | 4831 | 6012 | 1181 | | 57 | 35.4 | | | sand | rock | 2 | (1989) II | 250 |
| | | | | | | | | | SHALE | Source | | Burnham | |
| Paleocene | 6012 | 6533 | 521 | | 66 | 56.7 | | | silt | rock | 2.3 | (1989) III | 350 |
| | | | | | | 65.5 | | | | | | | |

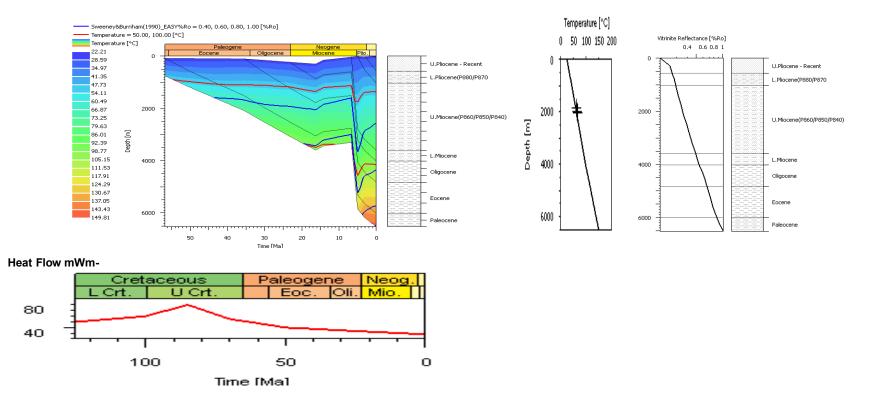


Fig. 5.16: Burial History chart showing isotherms, organic maturity and model calibration with temperature data for Kappa . 1 well in the Shallow Offshore depobelt of the Niger Delta.

5.7 Maturity and Hydrocarbon Generation

The temperature, maturation and kerogen transformation history derived for the four wells is summarized in figures 5.17, 5.18, 5.19 and 5.20. The calculated curves are plotted for the Paleocene, Eocene, Oligocene and Miocene layers to allow for comparison between different structural positions of these wells. It is noteworthy that important time steps of enhanced maturation and therefore, hydrocarbon generation depends on the structural positions of these wells and in particular on source rock depth.

5.7.1 Paleocene Source Rocks

The temperature, maturation and kerogen transformation history for Paleocene source rock intervals are shown in figure 5.17 a ó d. With the exception of Kappa-1 well, the calculated temperature evolution for the other three wells can be divided into three intervals. This includes; an initial progressive rise in temperature. Similarly, three clear stages of maturity evolution can be observed for the Paleocene source rocks. The observed stages include; an initial progressive maturity rise, an increased maturity rise and a rapid maturity rise (Fig. 5.17 a ó d). At Obig -1 well, the Paleocene source rock interval entered the oil window at 26 Ma and is currently in the gas generation phase (Ro = 1.8%), with a calculated transformation ratio (TR) of around 80%. At Akas ó 4, kerogen transformation into petroleum started at 12 Ma, when the source rocks entered the 100°C isotherm. The present day maturity level for the source rock is about 1.0 % Ro and 100% of the transformation potential has been exploited. At OpoS -4 well, the Paleocene source rock interval entered the oil window at 10 Ma and is currently within the late mature stage (Ro = 1.3 %), with a calculated transformation ratio of around 65%. At Kapp -1 well, two stages of temperature and maturity evolution are apparent for the

Paleocene source rocks. This include; an initial progressive rise in temperature and maturity and a later rapid rise in maturity. Here, the Paleocene source rocks entered the oil window at 19 Ma and is currently in the mid mature stage (Ro = 1.1%). The Paleocene source rocks have a calculated transformation ratio of about 33%.

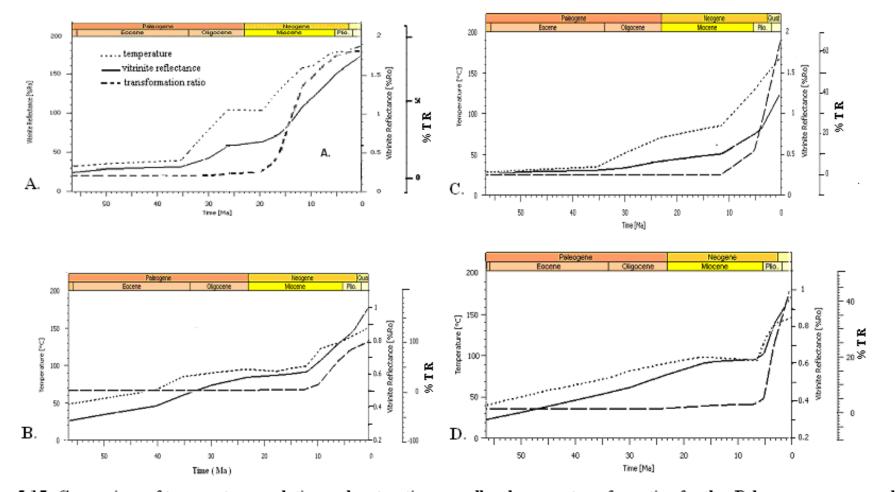


Figure 5.17. Comparison of temperature evolution and maturation as well as kerogen transformation for the Paleocene source rocks.
(A) Obig - 1 well (Central Swamp) (B) Akas - 4 well (Coastal Swamp) (C) Opos - 4 well (Coastal Swamp) and
(D) Kapp - 1 well (Shallow Offshore)

5.7.2 Eocene Source Rocks

The temperature, maturation and kerogen transformation history for Eocene source rock intervals are given in figures 5.18 a 6 d. Three clear stages of temperature and maturity evolution are observed for the Eocene source rocks with the exception of Kappa 6 1 well. At Obig -1 well, the onset of oil generation for the Eocene source rocks took place 21 Ma ago and is currently in the gas generation phase (Ro = 1.6%). At Akas 6 4 well, the kerogen transformation of Eocene source rocks into petroleum started at about 7 Ma, following the renewed subsidence. The present day maturity level for this source rock is about 0.78% and about 25% of the transformation potential has been exploited. At Opobo South 6 4 well, the onset of oil generation for the Eocene source rocks took place 9 Ma ago and the process of generation continues to present day (Ro = 1.1%) and the source rocks have not passed through the oil generation window. At Kappa -1 well, the Eocene source rocks started to generate oil at about 4 Ma and are still generating oil presently with a calculated transformation ratio of about 65%.

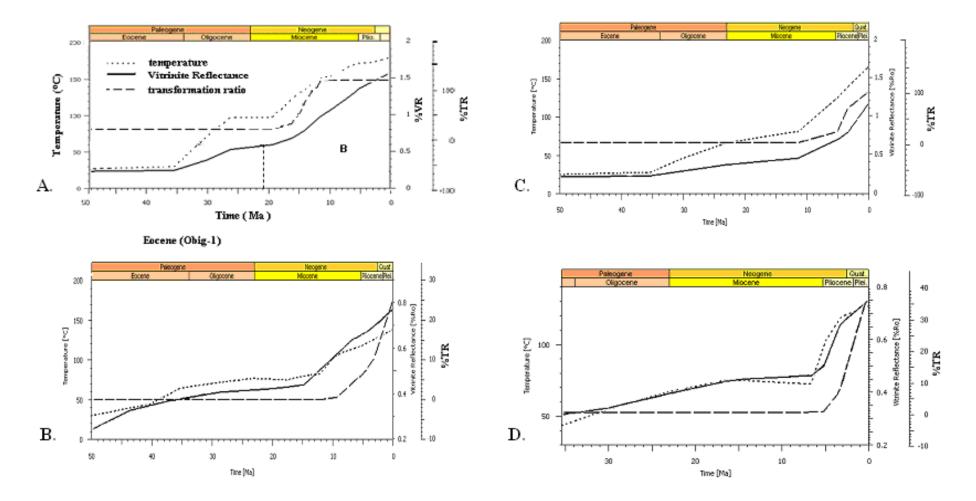


Figure 5.18. Comparison of temperature evolution and maturation as well as kerogen transformation for the Eocene source rocks.
(A) Obig - 1 well (Central Swamp) (B) Akas - 4 well (Coastal Swamp) (C) Opos - 4 well (Coastal Swamp) and
(D) Kapp - 1 well (Shallow Offshore)

5.7.3 Oligocene Source Rocks

The temperature, maturation and transformation history of Oligocene source rocks are shown in figures 5.19 a ó d. At Obig ó 1 well, the Oligocene sediments began to generate oil at 12 Ma ago. Oil generation within the Oligocene continued to present with Ro% of about 0.9%. At Akas ó 4, the Oligocene source rocks entered the oil window at about 1.5 Ma and its present day maturity level is about 0.66%. The Oligocene source rock interval has used only 25% of its transformation potential. At OpoS ó 4, well, the Oligocene sediments began to generate oil at 7 Ma, when the sediments entered the 100 °C isotherm. Oil generation within the Oligocene sediments continued to present with Ro% of about 1.0%. At Kappa-1 well, the basal part of the Oligocene entered the oil window at about 1 Ma with a Ro% of about 1.4%.

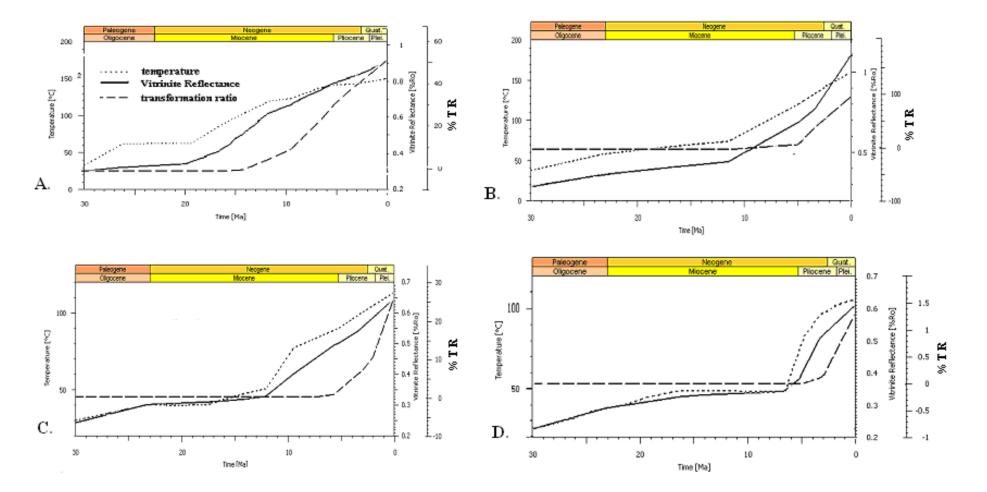


Figure 5.19. Comparison of temperature evolution and maturation as well as kerogen transformation for the Oligocene source rocks. (A) Obig - 1 well (Central Swamp) (B) Akas - 4 well (Coastal Swamp) (C) Opos - 4 well (Coastal Swamp) and (D) Kapp - 1 well (Shallow Offshore)

5.7.4 Lower Miocene Source Rocks

The temperature, maturation and transformation history of Miocene source rocks are shown in figures 5.20 a ó d. At Obig ó 1 well, the Lower Miocene entered the oil window at 3 Ma and its present day maturity level is about 0.75% Ro. At Opobo ó South ó 4, the lower Miocene and the basal part of the Upper Miocene entered the oil window at respectively at 3 and 1.5 Ma and their present maturity levels are 0.75 and 0.65% respectively.

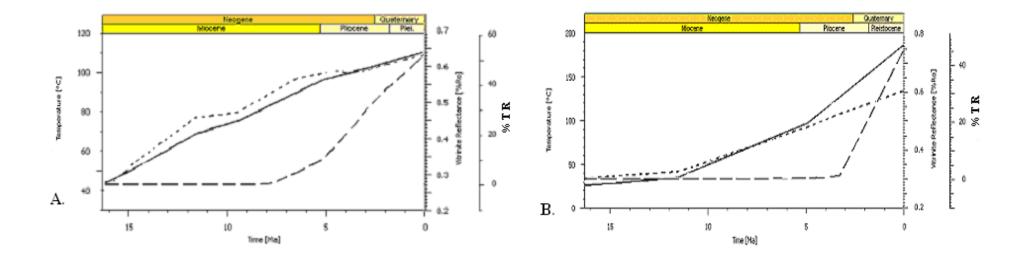


Figure 5.20. Comparison of temperature evolution and maturation as well as kerogen transformation for the Miocene source rocks. (A) Obig - 1 well (Central Swamp) (B) Opos - 4 well (Coastal Swamp)

CHAPTER SIX

6.0 DISCUSSION OF RESULTS AND CONCLUSION

6.1 Geothermal Gradients and Subsurface Temperature Distribution in the Niger Delta

The geothermal gradients pattern in the Eastern Niger Delta consists of a two leg dogleg geothermal gradients and a single leg geothermal gradients. The dogleg pattern is mostly observed in the Central and the Coastal Swamps while the single leg pattern is characterized by the Shallow Offshore. In the dogleg pattern, the upper or shallow thermal gradient belongs to the continental sandstones (Benin Formation), while the lower or deeper thermal gradient belongs to the marine / parallic section.

Generally geothermal gradients in the Niger Delta show a continuous but non linear relationship with depth, increasing with diminishing sand percentages. In the Niger Delta, geothermal gradients vary between 10 ó 24°C/Km in the continental section, and increases to 18 ó 45°C/Km in the deeper (marine / paralic) section. Sand percentages and geothermal gradients maps suggests that as sand percentages decreases eastwards, seawards, and northwards, geothermal gradients increaseøs. Thermal conductivities of the sediments also influence the geothermal pattern in the delta. The thermal conductivities decrease from about 2.3 W/mK in the continental sandstones to 1.56 W/mK in the paralic and continuous shaly sections.

Dogleg geothermal gradient patterns are characterized by a sudden departure of the temperature profile or the thermal gradient from the usual linear increase of the profile with depth. Hunt (1996) referred to this pattern as zones of variable gradient. The break in temperature profile can be likened the leg shape of a dog. Forest *et al.* (2007), observed some multi-linear, or dogleg geothermal gradient pattern in northern Gulf of Mexico. They suggested that the breaks in the temperature profile are often coincident with the top of overpressure zone or zone of thermal conductivity change. A dogleg feature may correspond to an unconformity associated with a large stratigraphic gap. Dogleg patterns have also been observed in vitrinite reflectance profiles in the Thrace Basin, North-western Turkey. (Huvaz *et al*, 2005. Some variations may occur within the dogleg patterns. It could be in the form of a three-leg pattern or double-dogleg pattern. Single leg geothermal gradient patterns are observed in areas with maximum thickness of the sandy Benin and Agbada Formations.

6.2 Factors Influencing Geothermal Anomalies and Heat Flow Variations in the Eastern Niger Delta

The factors influencing geothermal anomalies and heat flow variations in the Niger Delta include; variations in thermal conductivity, variations in sedimentation rates / sediment thicknesses, variable radiogenic heat production in basement rocks, variations in mantle heat flow, large scale water convection and advective flow of fluids.

(i) Variations in thermal conductivity and heat generation in the sediments.

Heat flow and geothermal anomalies are clearly influenced by lithology. Sands and shale of variable composition constitute the main litho-types in the Niger Delta. The thermal conductivities of these sediments range from 1.56 to 2.30 W/mK. In the study area, thermal conductivities generally decrease with depth. The sand percentage maps (Fig. 5.11a and 5.11b) shows that sand percentages generally decreases eastwards from the western part of the Eastern Coastal Swamp, and also to the Central Swamp and to the Shallow Offshore. The sand percentage variation is a reflection of the thermal conductivity variation in the sediments. A comparison of the heat flow map with the sand percentage maps has clearly shown that regions of low heat flow correspond with areas of high sand percentage or high thermal conductivity. The reason is because of the fact that sands are better conductors than shale and therefore will show lower heat flow. The sand percentage maps suggest that shale percentage increases as sand percentage decreases. This therefore implies that radiogenic heat production has a significant contribution to the total heat budget in these areas with a high proportion of shales. Clastic sediments such as shale are known to be rich in radiogenic heat producing elements, namely, thorium, uranium, and potassium. These radiogenic elements produce heat that is added to the total heat passing through the sedimentary column.

(ii) Variations in sedimentation rates / sediment thicknesses

An inverse relationship exists between sedimentation rate and seafloor heat flow (i.e., faster sedimentation rate, lower heat flow and vice versa) Nagihara and Jones (2005). The lower heat flow in the western parts of the eastern Coastal Swamp and the Shallow Offshore can be attributed to the Pliocene ó recent high sedimentation rates. The decrease in heat flow resulted from the addition of very thick, newer cold sediments on the surface. These new sediments absorbs heat as it rises through the sedimentary column, decreasing the amount of heat making it to the surface, as they try to equilibrate to the surrounding sediment temperature.

Sedimentation rates are usually calculated by dividing the sediment thickness by the age of the sediment and so they are related. Across the eastern part of the Niger Delta, sediment thicknesses decreases from about 12km in the west to about 3 km in the east corresponding roughly to an eastward increase in heat flow.

(iii) Fluid redistribution by migration of fluids

Fluid migration phenomena are observed worldwide in sedimentary basins (Hunt, 1990) and have been used to explain present day thermal anomalies (Andrew-Speed *et al.*1984, Chapman *et al.*1984, and Majorowicz 1989) The high heat flow in the eastern parts of the Central Swamp, Coastal Swamp and the Shallow Offshore as well as in the western part of the Central Swamp may be attributable to fault controlled fluid migration from deeply buried sediments such as the Akata Formation. A mechanism that may be responsible for high heat flow is the development of overpressure in shale. As sediment experiences compaction, pore water is squeezed out and migrates upward through younger, less compacted sediment or faults. If the flow is focused, along narrow conduits (e.g., faults), temperatures near the flow path become elevated as a result.

Large-scale water convection within the sandy Benin Formation has helped to reduce the heat flow flowing through the sediments especially in the western and central parts of the study area.

(iv) Basement heat flow

The result of magnetic intensity map shows that the magnetisation intensity of the Central Swamp is variable and strong (10 ó 110 nTesla), the Coastal Swamp is moderate (50 ó 90), and the Shallow Offshore is weak (0 ó 50). In the Central Swamp, magnetization highs, (>100 nTesla) occurs around Akata, Ibibio and Ekim fields, as well around Tabangh, Korokoro and Ofemini fields. Magnetization lows (< 50 nTesla) occur around Obigbo, Imo River, Odagwa and Oza fields. In the Shallow Offshore, the magnetization highs (>50 nTesla) occurs around KH-1 and KQ-1 wells, while magnetization lows occur around JD-1, JO-1 and JK-1 wells. Okubo *et al.* (2006) suggested that an aeromagnetic map generally reveals the subsurface structure of a sedimentary basin. According to them, the magnetic intensity map reveal the general distribution of magnetization near the surface as well as the thickness of the magnetic layer but does not give information on the depth. The magnetic intensity map therefore suggests that the Central Swamp and Coastal Swamp consists of thin Continental Crust except around areas with high magnetic intensity (>100 nTesla). It also suggests that the Shallow Offshore consists of a transitional crust.

According to Nagihara and Jones (2006), basement heat flow consists of two aspects; heat released from the mantle and heat due to radioactive heat production in basement rocks. In a continental margin setting, the extent of lithospheric stretching controls the heat flow experienced during a basins initiation. Generally, mantle heat flow decreases as the lithosphere cools. Radioactive heat production through decay of unstable elements (e.g., Uranium, Thorium and Potassium) from basement rocks also contributes to the total heat flow coming from the basement.

Thus the heat variations across the study area is a reflection of the heat contributions from the basement resulting from both lithospheric stretching and heat contributions from radioactive decay of unstable elements from basement rocks. Thus areas with thicker continental crusts experiences higher heat flow than areas with thinner continental and oceanic crust.

Okubo *et al* (2006) interpreted low magnetization as reflecting fractured or hydro-thermally altered zones caused by up flow of geothermal convection. According to them, in geothermal areas, hydrothermal alteration typically destroys the signature of volcanic rocks either by completely removing the iron or by converting magnetite to haematite, which has low magnetic susceptibility. The

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correlation of the magnetic intensity in the area with the heat flow estimates are shown in Profiles 1 (A \circ B), Profile 2(C \circ D) and Profile 3(E \circ F) (Figure 6.1).

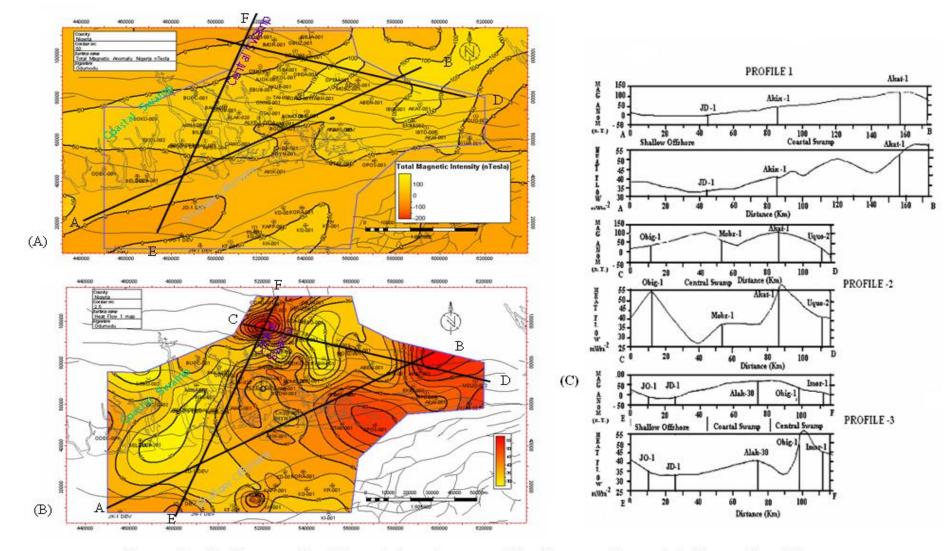


Figure 6.1 Profiles across Total Magnetic Intensity map and Heat Flow map of parts of the Eastern Niger Delta. (a) Magnetic Intensity map (b) Heat Flow map (c) Mag Anomaly and Heat Flow profiles

6.3 Burial History and Hydrocarbon Maturation Modelling

6.3.1 Source rocks

No available source rock samples were used in this study. However source rock analysis of Miocene and upper parts of the Oligocene have been described in some previous studies (Ekweozor and Okoye, Lambert ó Aikhionbare and Ibe, 1984; and Bustin, 1988). Some of these studies attributed the generated petroleum to be solely sourced from the shales of the Akata Formation with no contribution from the Agbada Formation while others suggest variable contributions from both formations and even from the deeper formation. The source rock maturity and hydrocarbon generation modelling results are shown in Figures 5.13 ó 5.20. A summary of the times when possible source rocks attained various levels of maturity in the studied wells is presented in table 6.10.

6.3.1.1 Paleocene source rocks

None of the wells penetrated into the Paleocene. The Paleocene was modelled as a potential source rock, using data from nearby wells especially from the flank. The TOC and Hydrogen index for Paleocene rocks are respectively 2.5% and 350 mgHCg⁻¹TOC respectively. The TOC value indicates a very good source potential while the hydrogen index suggests an oil source potential. The thermal maturity window of the Paleocene varies in different parts of the basin. The thermal maturity windows in these wells indicate that the Paleocene source rocks began to generate oil during the Oligocene and Miocene times. The Paleocene source rocks is inferred to be within; the gas generation window at Obigbo ó1, late mature window at Opobo South ó 4, mid mature window at Akaso ó 4 and Kappa ó 1. The predicted generated hydrocarbons are mainly gas and oil. The cumulative generation in the wells range from 0.54 ó 5.05 Mtons of oil and 0.95 ó 2.89 Mtons of gas.

| Well name | Formation or event name | Time of Early maturity | Time of Middle maturity | Time of Late maturity | Time of Main gas generation |
|-----------|----------------------------|------------------------------|-------------------------------|-----------------------------|-----------------------------------|
| Obigbo -1 | Palaeocene | 26 | 18 | 13 | 9 |
| | Eocene | 21 | 16 | 11 | 6 |
| | Oligocene | 12 | 8 | | |
| | Lower Miocene | 3 | | | |
| Akaso-4 | Palaeocene | 12 | 1 | | |
| | Eocene | 7 | | | |
| | Oligocene | 1.5 | | | |
| Opobo | Paleocene | 10 | 6 | 3 | |
| South - 4 | Eocene | 9 | 5 | 2 | |
| | Oligocene | 7 | 1 | | |
| | Lower Miocene | 3 | | | |
| | Upper Miocene | 1.5 | | | |
| Kappa-1 | Palaeocene | 19 | 5 | | |
| | Eocene | 4 | 3 | | |
| | Oligocene | 1 | | | |

Table 6.10. Times of different maturity levels attained by the modelled sourcerocks

6.3.1.2 Eocene source rocks

None of these wells were drilled in the Eocene source sediments. However Eocene source rocks were assumed as potential source rocks in this study because of the fact that they have been penetrated into in wells located in delta flanks. The Eocene apparently has attained levels of thermal maturity that differ in different time and spaces. Modelled maturity ranged from early maturity to main gas generation. The source rock maturity as indicated by TOC of 1.8 ó 2.3 % is generally fair to good. It has mixed kerogen type II and III. The Eocene source rocks attained proper maturity during the Miocene and Pliocene times. The Eocene source rocks are within; the gas generation window at Obigbo ó1, late mature window at Opobo South ó 4, middle mature window at Kappa ó1 and early mature window at Akaso ó 4. The model suggests a cumulative generation of 0.36 ó 1.47 Mtons of oil and 0.24 ó 0.77 Mtons of gas.

6.3.1.3 Oligocene source rocks

In the study area, it is only the upper part of the Oligocene has been penetrated because of the overpressured conditions of the shales at such great depths. Consequently, source rock analysis exists in literature for only the penetrated sections of the formation. It has mixed kerogen type II / III. Analytical results from literature shows the Total organic carbon content (TOC) varies from 1.6 ó 1.7 %, suggesting fair to good source potential whereas the hydrogen index range from 85 ó 150 suggesting a source potential for gas. The Oligocene sediments are currently within; the mid-mature oil window at Obigbo ó 1 and Opobo South ó 4 while it is in

the early mature zone at Akaso ó 4 and Kappa ó1. The cumulative generation varies from 0.0294 ó 1.05 Mtons of Gas and 0.0130 ó 1.52 Mtons of oil.

6.3.1.4 Miocene source rocks

Some of the wells penetrated into the Upper Miocene, Middle Miocene or the Lower Miocene. Substantial thickness of potential source rocks (shale) exists mainly in the Lower Miocene. The Upper and Middle Miocene serve as a primary reservoir. Source rock analysis for TOC in literature range from 0.80 ó 1.5 % indicating fair to poor source potential while the Hydrogen index of 57 ó 80 suggests a potential for gas. The Lower Miocene source rocks lies within the early ó mature zone at the Obigbo -1 and Opobo South ó 4 wells while it is not yet mature at Akaso ó 4 and Kappa ó 1 wells. The cumulative generation is 0.158 ó 0.196 Mtons for oil and 0.029 ó 0.037 for gas. The source rocks at the base of the Upper Miocene is within the early mature zone at the Opobo South ó 4 well while it is not yet near the oil window at the other three well locations.

The present modelling results reveals that higher levels of thermal maturity are attained in areas with high geothermal gradients and heat flow while the cooler areas exhibits lower levels of maturation. The onset of the oil window lies at 2859m at Obigbo ó 1 (Central Swamp), 3240m at Opobo South ó 4(Coastal Swamp), 4732m at Akaso ó 4(Coastal Swamp) and 4344 m at Kappa ó 1 (Shallow Offshore).

6.4 Implications of the Results

Results of this study have again confirmed the usefulness and applicability of reservoir and corrected bottom hole temperatures data for basin analysis studies. The result has also informed us on some new salient features on thermal gradients, heat flow and hydrocarbon maturation patterns in the Niger Delta. The thermal gradients increase eastwards, seawards and northwards from the Eastern Coastal Swamp. Thermal gradients in the Niger Delta also show a continuous and non linear relationship with depth. These increases in geothermal gradients reflects changes in thermal conductivities, increased shaliness, variation in sedimentation rates / sediments thicknesses, diagenetic differentiation, heat contributions from the basement and fluid redistribution in the sediments. The heat flow trend is a reflection of the geothermal gradients variations in the basin. This study may also give an insight into the regional hydrodynamic systems in the Niger Delta.

Geothermal gradient variations have a significant implication for source rock maturation. A comparison of a map of the study area showing oil and gas fields (Fig. 6.11) with the average geothermal gradient map of the study area (Fig. 5.4.) indicate certain trends. Very few oil and gas pools occur in the eastern parts while they are concentrated in the western parts of the study area. Geothermal gradients are higher in the eastern parts of the Coastal Swamp and in the western parts of Central Swamp. Several gas fields that occur within the study area include Obigbo and Afam gas fields in the Central Swamp. Other gas fields occurring within the study area include Alakiri and Soku gas fields. These gas fields usually occur with associated oil and for this fact the Niger Delta is usually described as a gas province associated with an unusual volume of oil. According to Turtle et al (2007), the Niger Delta is ranked as the twelfth position in recoverable gas reserves of all countries of the world and equally occupies an elevated rank in ultimate oil reserves. The large volume of gas in the Niger delta is primarily due to the presence of large quantity of terrestrial plant debris in the clastic sediments and secondly due to thermal maturation status.

Hydrocarbon maturation modelling have shown that potential source rocks in the Niger Delta such as the Paleocene, the Eocene, the Oligocene and the Lower Miocene have attained maturity status to generate hydrocarbons. The results also suggest that vast differences exist in the timing as well as the level of kerogen transformation into petroleum. The results also show that hydrocarbon maturation is greatly influenced by the variations in geothermal gradients.

6.5 Summary, Conclusion and Recommendations

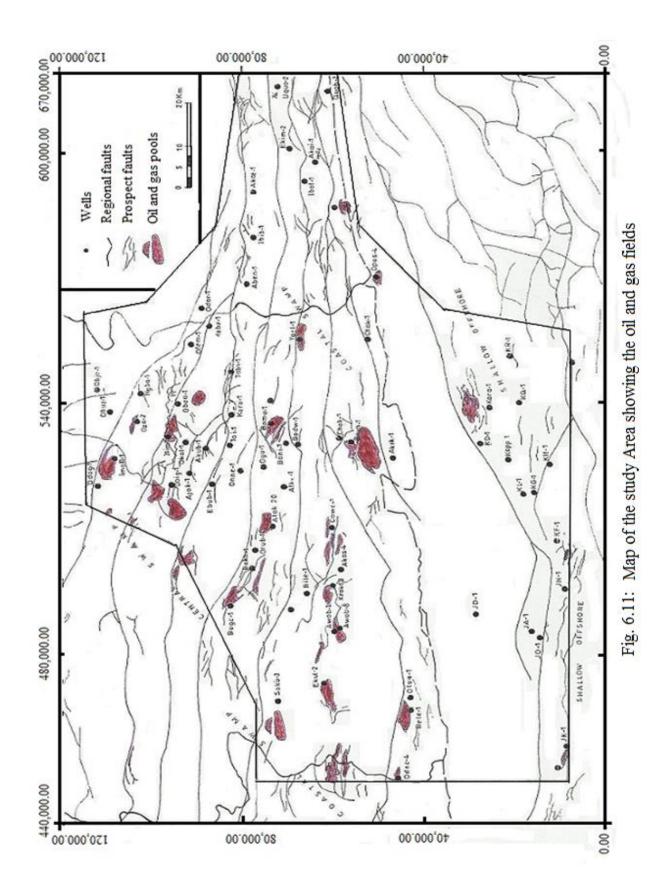
The thermal structure of the Eastern Niger Delta has been investigated so as to understand the thermal gradients pattern using reservoir and corrected bottomhole temperatures data from about seventy wells. The geothermal gradients show a continuous but non-linear relationship with depth, increasing with diminishing sand The geothermal gradients vary between 10-24 °C/km in the percentages. continental sandstones, and increases from 18 ó 45 °C/ km in the marine / paralic sections. Thermal gradients generally increase as sand percentages decreases eastwards and seawards. Thermal conductivities in the Niger Delta generally decrease with depth from 2.3W/mK in the continental sands to 1.56 W/mK in the paralic / continuous shaly sections. Thermal gradients in the Niger Delta are lithologically controlled. Minimum thermal gradients coincide with areas with maximum thickness of the sandy Agbada and Benin formations, while maximum values occur at the delta margins, where the deeper Akata Formation exerts a stronger influence.

Heat flow in the Eastern Niger Delta varies between 29 $m 6.55 \ mWm^{-2}$ (0.69 m 6 1.31 HFU), with an average of 42.5 mWm⁻². Higher heat flow values occur in the

eastern and northwestern parts of the study area. Lower heat flows characterize the eastern and central parts of the area.

Results of hydrocarbon maturation modelling suggest vast differences as regards to timing and levels of kerogen transformation to petroleum. It shows that the potential source rocks are mature to generate hydrocarbons. The depth to the oil generative window is deeper in the west and shallows to the east and northwest.

It is necessary to suggest that the data set be expanded for a more of comprehensive future studies. It is recommended that continuous temperature logs be ran for some of the wells so as to develop some statistical based correction factors for BHT data in the Niger Delta. It is also suggested that in future, vitrinite reflectance analysis be done for some of the cored source rock samples from these wells studied. The results will be used for geochemical data validation ó i.e. assessing the consistency of predicted vitrinite reflectance data with the measured data.



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| | APPEN | NDIX 1: BOTTOM | | PENDICE RATURE | |) DATA F | ROM LO | OG HEADE | R |
|-----|----------------|--------------------------|--------------------------|-------------------|---------|-----------|---------|----------|------|
| S/N | Well Names | Time circulation stopped | Time logger on bottom | Shut in time | BHT(oF) | Depth(FT) | BHT(oC) | Depth(m) | BHT© |
| | | | | | | 0 | | | |
| 1 | Abak - Enin -1 | | 30/08/1975 | 2 | 140 | 4520 | 60 | 1483 | 63 |
| | | 10-9-75/06:00 | 10-9-75/10:00 | 4 | 164 | 9010 | 73.33 | 2956 | 78 |
| | | | 10/9/1975 | 6 | 164 | 9010 | 73.33 | 2956 | 78 |
| | | | 10/9/1975 | 9 | 164 | 9010 | 73.33 | 2956 | 78 |
| | | | 10/9/1975 | 13 | 164 | 9010 | 73.33 | 2956 | 78 |
| | | | 10/9/1975 | 16 | 164 | 9010 | 73.33 | 2956 | 78 |
| | | 20/09/75/14:00 | 20-9-75/20:00 | 6 | 184 | 9438 | 84.44 | 3096 | 90 |
| | | | 22/09/1975 | 5 | 168 | 9408 | 75.56 | 3087 | 80 |
| | | | 22/09/1975 | 8 | 168 | 9408 | 75.56 | 3087 | 80 |
| | | | 22/09/1975 | 10 | 168 | 9408 | 75.56 | 3087 | 80 |
| 2 | Ajokpori-1 | | 19/02/1967 | | 108 | 4005 | 42.22 | 1314 | 44 |
| | | | 3/3/1967 | | 171 | 10837 | 77.22 | 3555 | 82 |
| | | | 5/3/1967 | | 173 | 11235 | 78.33 | 3686 | 83 |
| 3 | Akai-1 | 18-4-87/20:30 | 14-4-87/06:20 | | 132 | 5018 | 55.56 | 1646 | 59 |
| | | 02/05/87/22:15 | 3-5-87/10:30 | | 179 | 8697 | 81.67 | 2853 | 88 |
| | | 02/05/87/22:15 | 3-5-87/13:12 | | 179 | 8697 | 81.67 | 2853 | 88 |
| | | 5/13/1987 | 13-5-87/23:30 | | 195 | 9198 | 90.56 | 3018 | 97 |
| | | 16-5-87/22:00 | 19-5-87/09:54 | | 209 | 9943 | 98.33 | 3262 | 105 |
| 5 | Akata-1 | | 12/4/1953 | | 102 | 4065 | 38.89 | 1334 | 40 |
| | | | 4/6/1953 | | 150 | 7000 | 65.56 | 2297 | 70 |
| | | | 2/7/1953 | | 160 | 8185 | 71.11 | 2685 | 75 |
| | | | 22/07/1953 | | 239 | 10787 | 115 | 3539 | 124 |
| | | | 7/10/1953 | | 245 | 11104 | 118.3 | 3643 | 127 |
| | | | 7/10/1953 | | 245 | 11111 | 118.3 | 3645 | 127 |
| 6 | Akikigha-1 | 13-09-1987/13:00 | 13-9-87/18:41 | 5:41 | 112 | 5002 | 44.44 | 1641 | 46 |
| | | 25-9-87/03:00 | 25-9-87/20:30 | 17:30 | 159 | 9000 | 70.56 | 2953 | 75 |
| | | 25-9-87/03:00 | 25-9-87/15:45 | 12:45 | 156 | 9012 | 68.89 | 2957 | 73 |
| | | 25-9-87/03:00 | 25-9-87/10:00 | 7 | 154 | 9001 | 67.78 | 2953 | 72 |
| | | 25-9-87/03:00 | 26-9-87/00:15 | 21:15 | 163 | 9008 | 72.78 | 2955 | 78 |
| | | 5-10-87/17:00 | 6-10-87/04:00 | 12 | 187 | 10455 | 86.11 | 3430 | 72 |
| | | 25-9-87/03:00 | 26-9-87/02:30 | 11:30 | 232 | 14234 | 111.1 | 4670 | 109 |
| | | 25-9-87/07:45 | 26-9-87/02:30 | 6:45 | 232 | 14234 | 111.1 | 4670 | 109 |
| | | 5-10-87/17:00 | 6-10-87/14:15 | 21:15 | 194 | 10464 | 90 | 3433 | 96 |
| | | 5-10-87/17:00 | 6-10-87/09:00 | 16 | 191 | 10468 | 88.33 | 3434 | 94 |
| 7 | Akuba-1 | | 12/2/1967 | | 172 | 10380 | 77.78 | 3406 | 83 |
| 8 | Alakiri-East-1 | | 11/7/1977 | 4 | 107 | 4004 | 41.67 | 1314 | 44 |
| | ······ * | 19-11-77/11:00 | 20-11-77/12:30 | 25:30:00 | 170 | 9984 | 76.67 | 3276 | 82 |
| | | 19-11-77/11:00 | 20-11-77/16:00 | 27 | 174 | 9983 | 78.89 | 3275 | 84 |
| | | 19-11-77/23:00 | 20-11-77/7:15 | 8:15 | 163 | 9984 | 72.78 | 3276 | 78 |
| | | | 4/12/1979 | 3 | 190 | 11822 | 87.78 | 3879 | 94 |
| | | | 4/12/1979 | 12 | 190 | 11822 | 87.78 | 3879 | 94 |
| | | | 10/12/1977 | 4 | 192 | 11975 | 88.89 | 3929 | 95 |
| | | | 13/12/1977 | 5 | 196 | 12190 | 91.11 | 3999 | 97 |
| | | | 13/12/1977 | 10 | 196 | 12190 | 91.11 | 3999 | 97 |

| | | | 12/15/1977 | 12 | 218 | 12190 | 103.3 | 3999 | 111 |
|----|------------------------|----------------|------------------|-------|-----|-------|-------|------|-----|
| 9 | Alakiri-20 | | 11/11/1984 | | 174 | 9174 | 78.89 | 3010 | 84 |
| 10 | Awoba-1 | | 15/09/1965 | | 98 | 3512 | 36.67 | 1152 | 38 |
| - | | | 27/09/1965 | | 184 | 11978 | 84.44 | 3930 | 90 |
| | | | 28/09/1965 | | 184 | 11978 | 84.44 | 3930 | 90 |
| 11 | Awoba-8 | | 06/04/2003/08:25 | | 210 | 12877 | 98.89 | 4225 | 106 |
| | | | 11-5-03/04:00 | | 228 | 13964 | 108.9 | 4581 | 117 |
| | | | 13-5-03/04:45 | | 228 | 13964 | 108.9 | 4581 | 117 |
| | | 28-12-91/01:00 | 28-12-91/22:03 | 21:03 | 241 | 14997 | 116.1 | 4920 | 125 |
| 12 | Bakana-1 | | 13/04/1971 | | 94 | 3520 | 34.44 | 1155 | 35 |
| | | | 13/04/1971 | | 109 | 3520 | 42.78 | 1155 | 45 |
| | | | 22/04/1971 | | 154 | 9984 | 67.78 | 3276 | 72 |
| | | | 29/04/1971 | | 170 | 11037 | 76.67 | 3621 | 82 |
| 13 | Baniele-1 | 22-12-88/07:15 | 23-12-88/02:15 | 19 | 117 | 6006 | 47.22 | 1970 | 49 |
| | | | | | 152 | 8892 | 66.67 | 2917 | 71 |
| | | 9-1-89/03:00 | 9-1-89/22:15 | 19:15 | 155 | 8892 | 68.33 | 2917 | 72 |
| | | | | | 164 | 8894 | 73.33 | 2918 | 78 |
| | | 17-1-89/20:45 | 18-1-89/06:15 | 9:30 | 182 | 11097 | 83.33 | 3641 | 89 |
| | | | | | 190 | 11071 | 87.78 | 3632 | 94 |
| | | 31-1-89/02:45 | 01-02-89/06:51 | | 220 | 13075 | 104.4 | 4290 | 112 |
| 14 | Belema-1 | | 20/12/1980 | 6 | 110 | 4534 | 43.33 | 1488 | 45 |
| | | | 10/1/1981 | 12 | 170 | 10966 | 76.67 | 3598 | 81 |
| | | 10-01-81/12:00 | 11-01-81/5:00 | | 167 | 10966 | 75 | 3598 | 80 |
| | | | 12/1/1981 | 14 | 165 | 10976 | 73.89 | 3601 | 79 |
| | | | 4/2/1981 | | 202 | 13580 | 94.44 | 4455 | 101 |
| | | | 4/2/1981 | | 200 | 13606 | 93.33 | 4464 | 100 |
| | | | 12/2/1981 | 11:15 | 163 | 10975 | 72.78 | 3601 | 78 |
| | | | 15-12-91/20:23 | | 191 | 12400 | 88.33 | 4068 | 94 |
| 15 | Bille-1 | | 4/11/1971 | 2 | 110 | 5042 | 43.33 | 1654 | 45 |
| | | | 4/11/1971 | 6 | 110 | 5042 | 43.33 | 1654 | 45 |
| | | | 5/11/1971 | 11 | 110 | 5042 | 43.33 | 1654 | 45 |
| | | | 18/11/1971 | 4 | 171 | 11304 | 77.22 | 3709 | 82 |
| | | | 19/11/1971 | 15 | 171 | 11300 | 77.22 | 3707 | 82 |
| | | | 22/11/1971 | 29 | 171 | 8400 | 77.22 | 2756 | 82 |
| 16 | Bodo-WEST-1 | | | | | | | | |
| 17 | Bomu-1 | | 25/2/1958 | | 90 | 1710 | 32.22 | 561 | 33 |
| | | | 8/3/1958 | | 125 | 6491 | 51.67 | 2130 | 54 |
| | | | 20/03/1958 | | 137 | 7569 | 58.33 | 2483 | 61 |
| | | | 23/03/1958 | | 154 | 8947 | 67.78 | 2935 | 71 |
| | ļ | | 28/03/1958 | | 154 | 8948 | 67.78 | 2936 | 71 |
| | ļ | | 9/4/1958 | | 182 | 10262 | 83.33 | 3367 | 89 |
| 18 | Bonny-North-1 | | 6/2/1964 | | 187 | 7815 | 86.11 | 2564 | 92 |
| | ├ ──── ├ | | 6/2/1964 | | 187 | 7824 | 86.11 | 2567 | 92 |
| | ├ ──── ├ | | 7/2/1964 | | 185 | 11883 | 85 | 3899 | 91 |
| | Dec est | | 17/02/1964 | | 185 | 11895 | 85 | 3903 | 91 |
| 19 | Buguma Creek-1 | | 21/03/1960 | | 120 | 6982 | 48.89 | 2291 | 51 |
| | | | 22/03/1960 | | 150 | 6970 | 65.56 | 2287 | 70 |
| | | | 22/03/1960 | | 122 | 6975 | 50 | 2288 | 52 |

| | 1 | | 22/03/1960 | | 120 | 6976 | 48.89 | 2289 | 50 |
|----|------------------------|----------------|----------------|----------|-----|-------|-------|-------|-----|
| | | | 5/4/1960 | | 220 | 10744 | 104.4 | 3525 | 112 |
| | | | 14/04/1960 | | 186 | 11997 | 85.56 | 3936 | 92 |
| | | | 12/4/1960 | | 196 | 10025 | 91.11 | 3289 | 97 |
| | | | 18/04/1960 | | 196 | 12140 | 91.11 | 3983 | 97 |
| | | | 18/04/1960 | | 196 | 12145 | 91.11 | 3985 | 97 |
| 20 | Cawthorne Channel-1 | | 2/11/1963 | | 156 | 10050 | 68.89 | 3297 | 73 |
| | 0 | | 2/11/1963 | | 156 | 10032 | 68.89 | 3291 | 73 |
| | | | 2/12/1963 | | 156 | 10025 | 68.89 | 3289 | 73 |
| | | | 2/24/1963 | | 196 | 12428 | 91.11 | 4077 | 97 |
| | | | 2/25/1963 | | 196 | 12551 | 91.11 | 4118 | 97 |
| | | | 2/27/1963 | | 228 | 12901 | 108.9 | 4233 | 117 |
| | | | 3/1/1963 | | 228 | 12908 | 108.9 | 4235 | 117 |
| | | | 3/1/1963 | | 230 | 12907 | 110 | 4235 | 118 |
| | | | 3/4/1963 | | 225 | 13140 | 107.2 | 4311 | 115 |
| | | | 18-06-95/07:51 | | 265 | 11130 | 129.4 | 3652 | 139 |
| | | | 18-06-95/18:08 | | 265 | 11132 | 129.4 | 3652 | 139 |
| 21 | Chobie-1 | | 3/19/1980 | 4 | 110 | 4504 | 43.33 | 1478 | 45 |
| | | | 4/1/1980 | 12 | 184 | 11001 | 84.44 | 3609 | 90 |
| | | | 4/2/1980 | 12 | 190 | 11000 | 87.78 | 3609 | 94 |
| | | 01-04-80/12:00 | 02-04-80/02:00 | 2 | 186 | 11000 | 85.56 | 3609 | 91 |
| | | | 5/2/1980 | 16 | 212 | 12720 | 100 | 4173 | 108 |
| | | 01-04-80/16:00 | 2-05-80/02:00 | 10 | 201 | 12720 | 93.89 | 4173 | 101 |
| | | | 4/28/1980 | | 215 | 13200 | 101.7 | 4331 | 110 |
| | | 03-05-80/11:30 | 04-05-80/03:00 | 3:30 | 206 | 12718 | 96.67 | 4173 | 114 |
| 22 | Ebubu-1 | | | | | | | | |
| 22 | Ekim-2 | 04-11-86/17:00 | 05-11-86/11:00 | 18 | 115 | 4601 | 46.11 | 1510 | 48 |
| 23 | ERIII-2 | 04-11-86/17:00 | 05-11-86/18:00 | 25 | 115 | 4601 | 46.11 | 1510 | 48 |
| | | 21-11-86/11:00 | 22-11-86/19:14 | 26:14:00 | 190 | 9024 | 87.78 | 2961 | 93 |
| | | 21-11-86/11:30 | 22-11-86/08:50 | 21:20 | 180 | 9030 | 82.22 | 2963 | 88 |
| | | 08-12-86/19:15 | 09-12-86/06:30 | 11:15 | 216 | 10707 | 102.2 | 3513 | 110 |
| | | 14-12-86/04:30 | 14-12-86/14:40 | 10:10 | 224 | 11027 | 106.7 | 3618 | 115 |
| | | 15-12-86/22:00 | 16-12-86/11:49 | 13:49 | 232 | 11027 | 111.1 | 3618 | 119 |
| 24 | Elmlo | | | | | | | | |
| 24 | Ekulama-2 Ibibio-1 | | 5/11/1959 | | 125 | 4504 | 51.67 | 1478 | 55 |
| 25 | 101010-1 | | 6/11/1959 | | 125 | 3650 | 60 | 1478 | 63 |
| | | | 27/11/1959 | | 140 | 9159 | 76.67 | 3005 | 81 |
| | | | 28/11/1959 | | 170 | 8500 | 77.22 | 2789 | 82 |
| 26 | Ibotio-1 | | 17/06/195 | | 100 | 516 | 37.78 | 169.3 | 39 |
| 20 | 10010-1 | | 26/06/1955 | | 129 | 3520 | 53.89 | 1155 | 57 |
| | | | 28/06/1955 | | 131 | 4355 | 55 | 1429 | 58 |
| | | | 12/7/1955 | | 163 | 7559 | 72.78 | 2480 | 79 |
| | | | 23/07/1955 | | 188 | 9060 | 86.67 | 2972 | 93 |
| 27 | Imo River-1 | | | | | | | | |
| 28 | Isimiri-1 | | 17/03/1964 | | 153 | 3061 | 67.22 | 1004 | 71 |
| | | | 31/03/1964 | | 155 | 10030 | 68.33 | 3291 | 72 |

| | | | 16/04/1964 | | 192 | 11889 | 88.89 | 3901 | 95 |
|----|--------------|----------------|----------------------|-------|-----|-------|-------|-------|-----|
| 29 | Korokoro-2 | | 11/8/1962 | | 112 | 4019 | 44.44 | 1319 | 46 |
| | Reference 2 | | 29/08/1962 | | 160 | 10950 | 71.11 | 3593 | 75 |
| 30 | Krakama-2 | | 24/03/1962 | | 102 | 2495 | 38.89 | 818.6 | 40 |
| | | | 2/5/1962 | | 146 | 8503 | 63.33 | 2790 | 67 |
| | | | 15/02/1972 | | 158 | 8144 | 70 | 2672 | 74 |
| | | | 23/09/1958 | | 178 | 11076 | 81.11 | 3634 | 86 |
| | | | 19/03/1972 | | 166 | 11576 | 74.44 | 3798 | 79 |
| 31 | Minama-1 | | 19/01/1967 | | 144 | 11250 | 62.22 | 3691 | 66 |
| 32 | Mobazi-1 | | 28/12/1960 | | 104 | 3830 | 40 | 1257 | 41 |
| 33 | Ngboko-1 | | | | 152 | 9047 | 66.67 | 2968 | 71 |
| | | | | | 158 | 9495 | 70 | 3115 | 74 |
| 34 | Obeaja-1 | | 30/01/1976 | 12 | 172 | 7738 | 77.78 | 2539 | 83 |
| 35 | Obeakpu-1 | | 14/10/1975 | 2 | 120 | 3762 | 48.89 | 1234 | 51 |
| | | | 25/10/1975 | 19 | 152 | 8100 | 66.67 | 2657 | 71 |
| | | | 25/10/1975 | 19.5 | 152 | 8100 | 66.67 | 2657 | 71 |
| | | | 25/10/1975 | 11 | 152 | 8268 | 66.67 | 2713 | 71 |
| | | 24-10-75/21:00 | 25-10-75:04:00 | 7 | 152 | 8284 | 66.67 | 2718 | 71 |
| | | | | 15 | 152 | 8276 | 66.67 | 2715 | 71 |
| | | | | 19.5 | 153 | 8285 | 67.22 | 2718 | 71 |
| 36 | Obigbo-1 | | 11/8/1958 | 2 | 120 | 3762 | 48.89 | 1234 | 51 |
| | | | 11/8/1958 | | 214 | 10280 | 101.1 | 3373 | 108 |
| | | | 11/8/1958 | | 224 | 10543 | 106.7 | 3459 | 114 |
| | | | 11/10/1974 | | 230 | 10782 | 110 | 3537 | 118 |
| 37 | Obuzor-1 | | 12/9/1971 | | 110 | 2993 | 43.33 | 982 | 45 |
| | | | 20/09/1971 | | 179 | 8525 | 81.67 | 2797 | 88 |
| 38 | Odagwa-1 | | | 3 | 100 | 3014 | 37.78 | 988.8 | 39 |
| | | 1-10-77/8:30 | 18-10-77/03:30 | | 145 | 7519 | 62.78 | 2467 | 67 |
| | | 17-10-77/08:30 | 17-10-77/02:40 | 7:10 | 140 | 7518 | 60 | 2467 | 63 |
| | | 17-10-77/08:30 | 17-10- 1977/06:20 | | 140 | 7521 | 60 | 2468 | 63 |
| | | 04-11-77/07:00 | 04-11-77/14:00 | 7:00 | 140 | 7521 | 60 | 2468 | 63 |
| | | 04-11-77/07:00 | 04-11-77/14:00 | 7:00 | 178 | 9490 | 81.11 | 3114 | 86 |
| | | 04-11-77/07:00 | 04-11-77/23:30 | 13:30 | 181 | 9498 | 82.78 | 3116 | 89 |
| | | | | | 182 | 9490 | 83.33 | 3114 | 89 |
| 20 | Odeama- | | 17/03/1981 | 22:30 | 172 | 10912 | 77.78 | 3580 | 83 |
| 39 | Creek-4 | | 19/03/1981 | 6:00 | 172 | 11388 | 80.56 | 3736 | 85 |
| | | 19-3-81/06:00 | 20-3-81/08:15 | 14:15 | 177 | 11388 | 81.11 | 3736 | 86 |
| | | 17-3-01/00.00 | 3/4/1981 | 19:30 | 200 | 13143 | 93.33 | 4312 | 100 |
| | | | 7/4/1981 | 19:30 | 200 | 13143 | 95.56 | 4512 | 113 |
| | | | 7/4/1981 | 16:00 | 204 | 13775 | 95.50 | 4519 | 113 |
| | | 6-4-81/16:00 | 7-4-81/17:30 | 10.00 | 200 | 13773 | 98.89 | 4503 | 115 |
| 40 | Odana Urat 1 | 0 | 10/8/1971 | 8 | 130 | 4785 | 54.44 | 1570 | 57 |
| 40 | Odoro-Ikot-1 | | 10/8/1971 | 12:00 | 130 | 4785 | 54.44 | 1570 | 57 |
| | | | 10/8/1971 | 38 | 130 | 4785 | 54.44 | 1570 | 57 |
| | | | 25/08/1971 | 4 | 152 | 8401 | 66.67 | 2756 | 71 |
| | | | $\Delta J/U0/17/1$ | 4 | 154 | 0401 | 00.07 | 2150 | / 1 |
| | | | 25/08/1971 | 5 | 152 | 8501 | 66.67 | 2789 | 71 |

| 41 | Ofemini-1 | | | | | | | | |
|----|-------------------|------------------|------------------|-------|-----|-------|-------|-------|-----|
| 42 | Ogu-1 | | 12/2/1965 | 3 | 163 | 8481 | 72.78 | 2782 | 78 |
| | | | 12/2/1965 | 6 | 163 | 9982 | 72.78 | 3275 | 78 |
| | | | 2/4/1973 | 6 | 184 | 11101 | 84.44 | 3642 | 90 |
| | | | 20/04/1973 | 10 | 216 | 12323 | 102.2 | 4043 | 110 |
| | | | 28/04/1973 | | 242 | 12834 | 116.7 | 4211 | 125 |
| 43 | Okiori-1 | | 8/10/1975 | 3 | 100 | 4050 | 37.78 | 1329 | 39 |
| | | | 15/10/1975 | 10 | 148 | 9509 | 64.44 | 3120 | 68 |
| | | | 15/10/1975 | 14 | 148 | 9509 | 64.44 | 3120 | 68 |
| | | | 15/10/1975 | 18 | 148 | 9509 | 64.44 | 3120 | 68 |
| | | | 23/10/1975 | 10 | 160 | 11496 | 71.11 | 3772 | 75 |
| | | | 23/10/1975 | 12 | 160 | 11496 | 71.11 | 3772 | 75 |
| | | | 23/10/1975 | 16 | 160 | 11496 | 71.11 | 3772 | 75 |
| 44 | Okoloma-1 | | | | | | | | |
| 45 | Okoroba-1 | 10-12-90/02:30 | 10-12-90/09:01 | 6:31 | 93 | 4426 | 33.89 | 1452 | 35 |
| 46 | Olua-1 | 2-2-79/11:45 | 2/1/1979 | | 105 | 3492 | 40.56 | 1146 | 42 |
| | | 19/01/1979/17:00 | 20/01/1979/04:30 | 11:30 | 160 | 10211 | 71.11 | 3350 | 75 |
| | | | 20/01/1979 | 16 | 166 | 10212 | 74.44 | 3350 | 79 |
| | | | 20/01/1979 | 24 | 168 | 10213 | 75.56 | 3351 | 81 |
| | | 02/01/1979/11:45 | 02/01/1979/19:15 | 7:30 | 192 | 12368 | 88.89 | 4058 | 95 |
| | | 02/01/1979/11:45 | 02/01/1979/21:30 | 9:45 | 196 | 12367 | 91.11 | 4057 | 97 |
| | | | 2/1/1979 | 12 | 200 | 12367 | 93.33 | 4057 | 99 |
| | | 2-2-79/11.45 | 2-2-79/10:30 | | 202 | 12368 | 94.44 | 4058 | 101 |
| 47 | Onne-1 | | 22/03/1965 | | 98 | 3505 | 36.67 | 1150 | 38 |
| | | | 2/3/1965 | | 154 | 10370 | 67.78 | 3402 | 72 |
| | | | 3/4/1965 | | 154 | 10370 | 67.78 | 3402 | 72 |
| | | | 3/4/1965 | | 154 | 10380 | 67.78 | 3406 | 72 |
| | | | 4/3/1965 | | 154 | 10384 | 67.78 | 3407 | 72 |
| | | | 5-10-92/19:20 | | 174 | 9692 | 78.89 | 3180 | 84 |
| 48 | Opobo-South- 4 | | 4/8/1974 | | 197 | 9517 | 91.67 | 3122 | 99 |
| | - | | 28/08/1974 | | 183 | 9953 | 83.89 | 3265 | 90 |
| | | | 15/09/1974 | | 200 | 11821 | 93.33 | 3878 | 100 |
| 49 | Orubiri-4 | | 6/2/1972 | 3.5 | 102 | 4040 | 38.89 | 1325 | 40 |
| | | | 14/02/1972 | 3 | 160 | 9401 | 71.11 | 3084 | 75 |
| | | | 15/02/1972 | 24 | 160 | 9400 | 71.11 | 3084 | 75 |
| | | | 16/02/1972 | 13 | 160 | 9402 | 71.11 | 3085 | 75 |
| 50 | Otakikpo-1 | | | | | | | | |
| 51 | Oza-2 | | 11/5/1962 | | 92 | 1004 | 33.33 | 329.4 | 34 |
| | | | 19/05/1962 | | 116 | 7000 | 46.67 | 2297 | 49 |
| | | | 24/05/1962 | | 140 | 8999 | 60 | 2952 | 63 |
| | | | 4/6/1962 | | 190 | 10997 | 87.78 | 3608 | 94 |
| 52 | Qua-Ibo-1 | | 26/01/1960 | | 122 | 5179 | 50 | 1699 | 53 |
| | | | 4/2/1960 | | 165 | 8473 | 73.89 | 2780 | 79 |
| | | | 9/2/1960 | | 200 | 9496 | 93.33 | 3115 | 100 |
| 53 | Soku-3 | | 3/1/1963 | | 104 | 2523 | 40 | 827.8 | 41 |
| | | | 14/01/1963 | | 142 | 10074 | 61.11 | 3305 | 64 |
| | | | 25/01/1963 | | 167 | 12377 | 75 | 4061 | 80 |
| 54 | Tabangh-1 | | 6/10/1962 | | 100 | 3522 | 37.78 | 1156 | 39 |

| | 1 | 24/10/1962 | | 150 | 9995 | 65.56 | 3279 | 70 |
|----|-----------|----------------|----|-----|-------|-------|-------|----|
| | | 12/11/1962 | | 130 | 11623 | 76.67 | 3813 | 82 |
| | Tai-2 | 22/11/1963 | 6 | 160 | 9600 | 71.11 | 3150 | 75 |
| | 1 al-2 | 6/12/1973 | 6 | 170 | 11339 | 76.67 | 3720 | 82 |
| 56 | Uquo-2 | 10/5/1971 | 0 | 124 | 4012 | 51.11 | 1316 | 53 |
| 50 | Oquo-2 | 16/05/1971 | | 150 | 7185 | 65.56 | 2357 | 70 |
| | | 17/05/1971 | | 150 | 7185 | 65.56 | 2357 | 70 |
| | | 17/05/1971 | | 150 | 7189 | 65.56 | 2350 | 70 |
| | | 18/05/1971 | 15 | 149 | 7139 | 65 | 2342 | 69 |
| | | 24/05/1971 | 12 | 180 | 8906 | 82.22 | 2922 | 88 |
| | | 26/05/1971 | 12 | 180 | 8915 | 82.22 | 2925 | 88 |
| | | 26/05/1971 | 8 | 180 | 8885 | 82.22 | 2915 | 88 |
| | | 26/05/1971 | | 180 | 8895 | 82.22 | 2918 | 88 |
| 57 | Yomene-1 | 2/4/1962 | | 90 | 2018 | 32.22 | 662.1 | 33 |
| 51 | Tomene-1 | 15/04/1962 | | 161 | 9480 | 71.67 | 3110 | 76 |
| | | 15/04/1962 | | 161 | 9484 | 71.67 | 3112 | 76 |
| 58 | Yorla-1 | 4/11/1970 | | 105 | 4514 | 40.56 | 1481 | 43 |
| - | | 25/11/1970 | | 188 | 10500 | 86.67 | 3445 | 93 |
| | | 18/11/1970 | 12 | 190 | 11900 | 87.78 | 3904 | 94 |
| | | 18/11/1970 | 18 | 190 | 11888 | 87.78 | 3900 | 94 |
| 59 | KH-1 | 8/1/1967 | | 107 | 4035 | 41.67 | 1324 | 44 |
| | | 21/01/1967 | | 189 | 10976 | 87.22 | 3601 | 93 |
| | | 22/01/1967 | | 189 | 10973 | 87.22 | 3600 | 93 |
| | | 28/01/1967 | | 189 | 10976 | 87.22 | 3601 | 93 |
| 60 | KL-1 | 28/01/1967 | | 110 | 3021 | 43.33 | 991.1 | 45 |
| | | 6/2/1967 | | 188 | 10224 | 86.67 | 3354 | 91 |
| 61 | Koronama1 | 18/03/1983 | | 188 | 10575 | 86.67 | 3469 | 91 |
| 62 | KR-1 | 31/05/1971 | 3 | 101 | 3015 | 38.33 | 989.2 | 39 |
| | | 9/6/1971 | 25 | 164 | 8989 | 73.33 | 2949 | 78 |
| 63 | KG-1 | 26/11/1966 | | 107 | 4008 | 41.67 | 1315 | 44 |
| | | 11/12/1966 | | 191 | 10870 | 88.33 | 3566 | 94 |
| 64 | KF-1 | 27/02/1971 | | 109 | 3498 | 42.78 | 1148 | 45 |
| | | 27/02/1971 | | 109 | 3506 | 42.78 | 1150 | 45 |
| | | 11/3/1971 | | 180 | 10485 | 82.22 | 3440 | 88 |
| | | 11/3/1971 | | 180 | 10495 | 82.22 | 3443 | 88 |
| | | 11/3/1971 | | 180 | 10497 | 82.22 | 3444 | 88 |
| | | 12/3/1971 | | 180 | 10497 | 82.22 | 3444 | 88 |
| 65 | JO-1 | 31/01/1971 | | 118 | 4040 | 47.78 | 1325 | 50 |
| | | 16/02/1971 | 10 | 182 | 9954 | 83.33 | 3266 | 89 |
| 66 | JD-1 | 1/7/1966 | | 110 | 3470 | 43.33 | 1138 | 45 |
| | | 14/07/1966 | | 160 | 10986 | 71.11 | 3604 | 75 |
| 67 | JA-1 | 30/01/1965 | | 102 | 3498 | 38.89 | 1148 | 40 |
| | | 15-16/02/1965 | | 180 | 10998 | 82.22 | 3608 | 88 |
| | | 17/02/1965 | | 180 | 10999 | 82.22 | 3609 | 88 |
| 68 | JK-1 | 28/03/1967 | | 110 | 3013 | 43.33 | 988.5 | 45 |
| | | 4/4/1967 | | 182 | 9083 | 83.33 | 2980 | 89 |
| 69 | JN-1 | 29/10/1971 | | 115 | 4016 | 46.11 | 1318 | 48 |
| | | 8/11/1971 | | 194 | 10972 | 90 | 3600 | 96 |

APPENDIX II

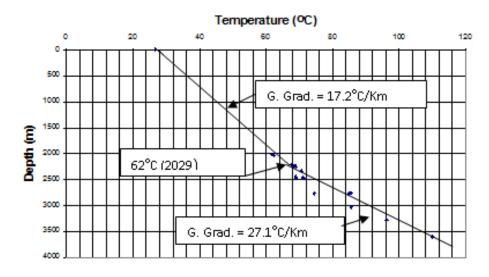


Figure 1: Temperature - Depth plot of the Bodo- West field

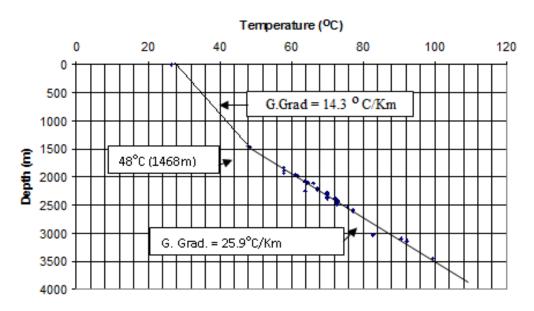
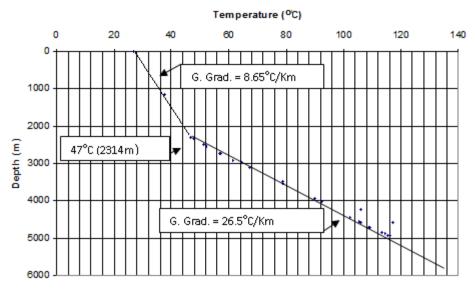
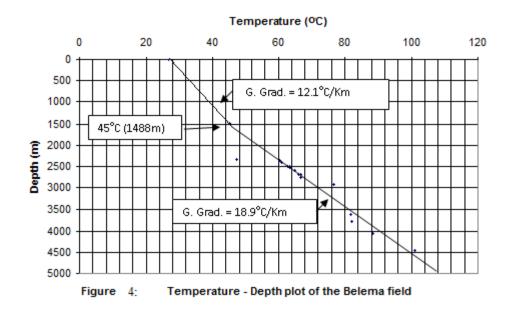


Figure 2: Temperature-Depth plot for Bomu field







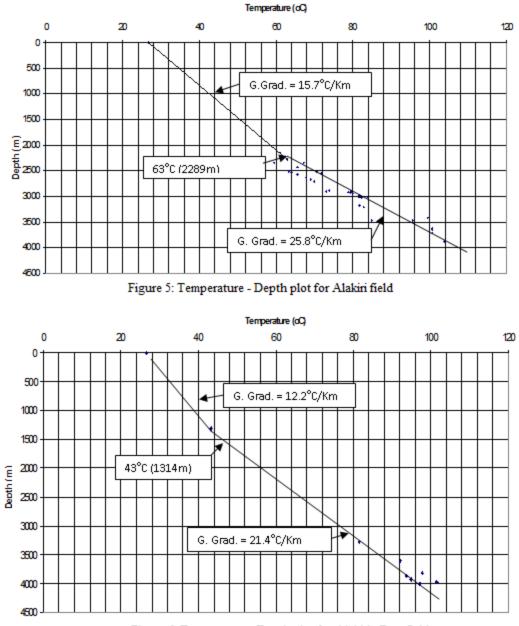
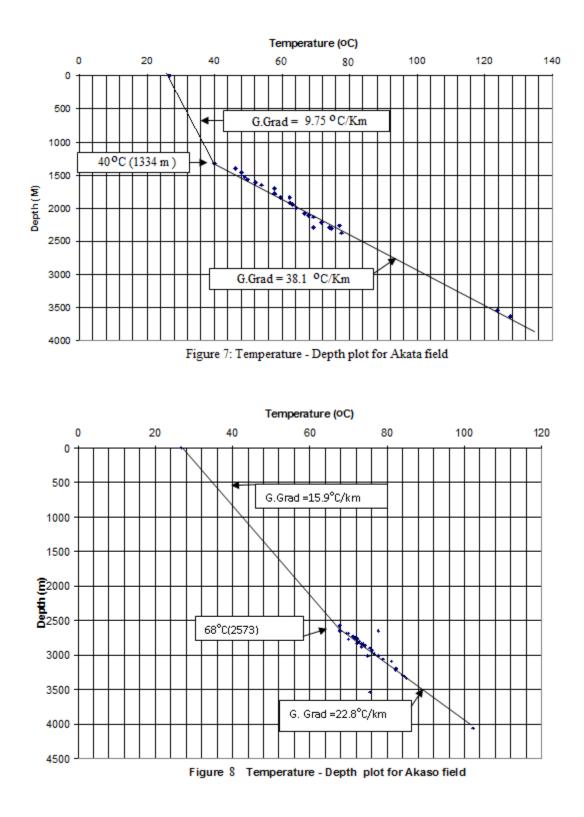
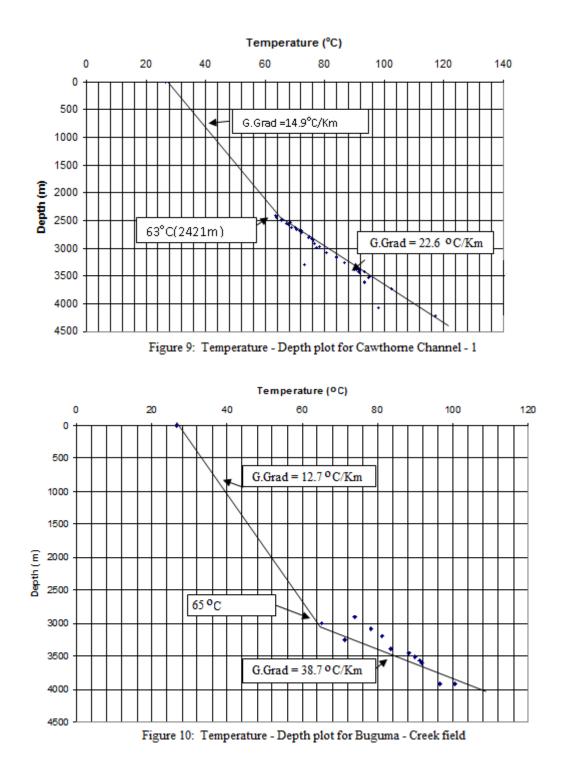
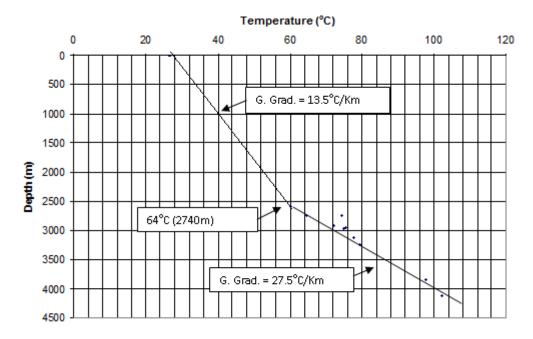
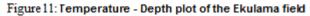


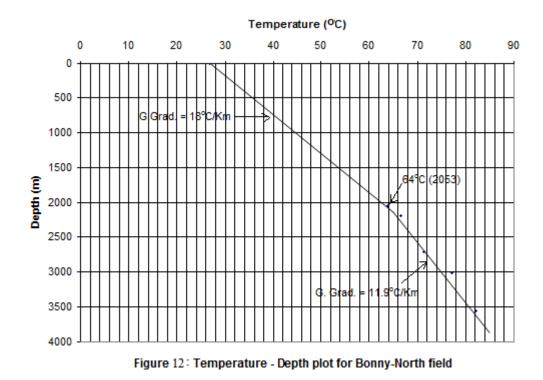
Figure 6: Temperature - Depth plot for Alakiri - East field

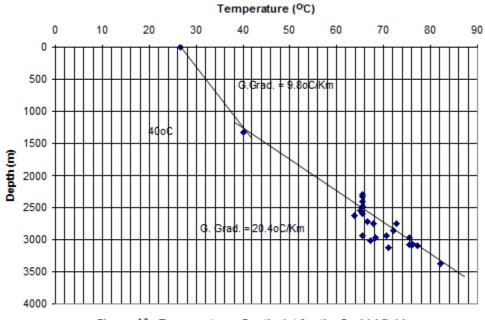


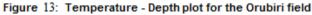












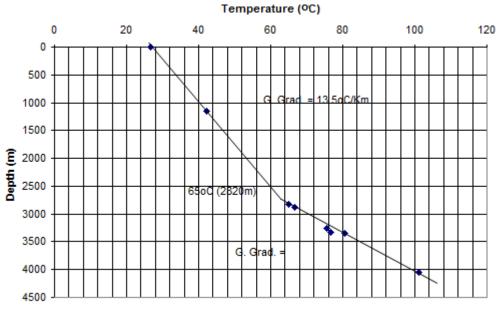
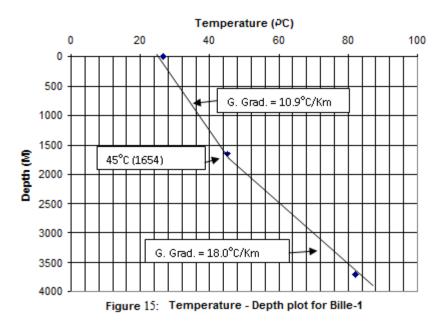
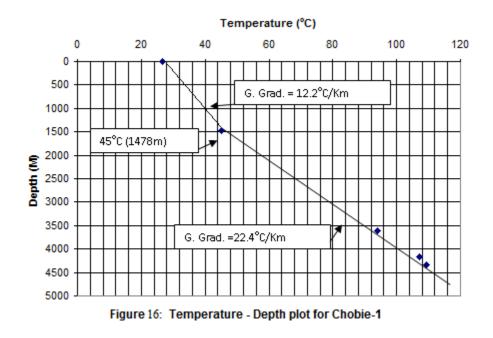


Figure 14: Temperature - Depth plot for the Olua field





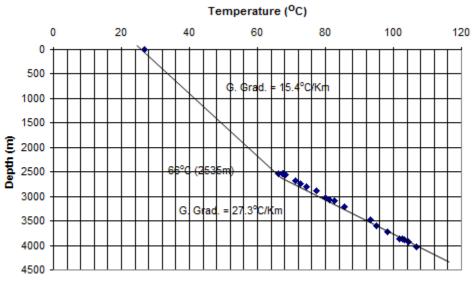


Figure 17: Temperature - Depth plot for Odeama Creek field

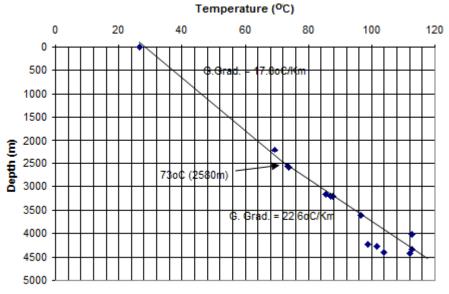
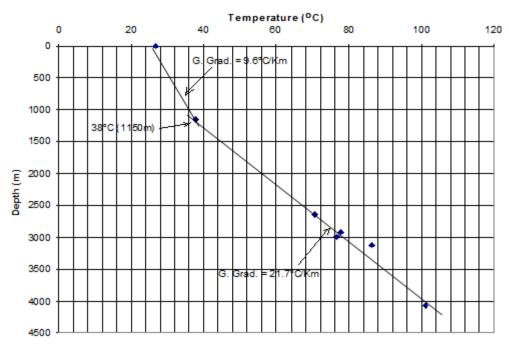
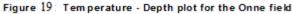


Figure 18: Temperature - Depth plot for Krakama field.





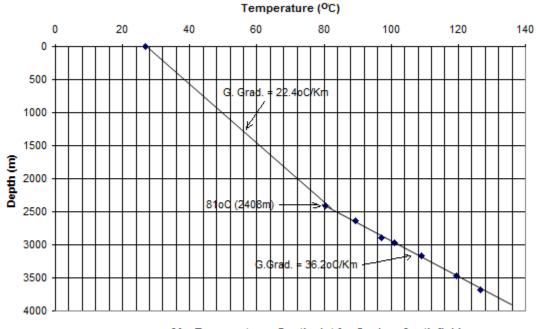


Figure 20: Temperature - Depth plot for Opobo - South field

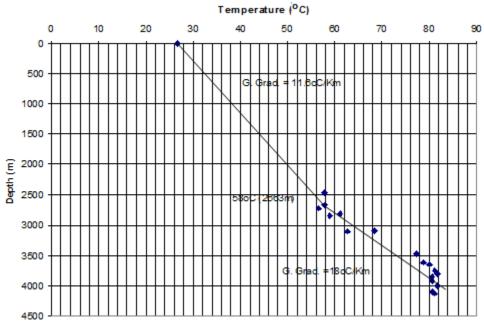
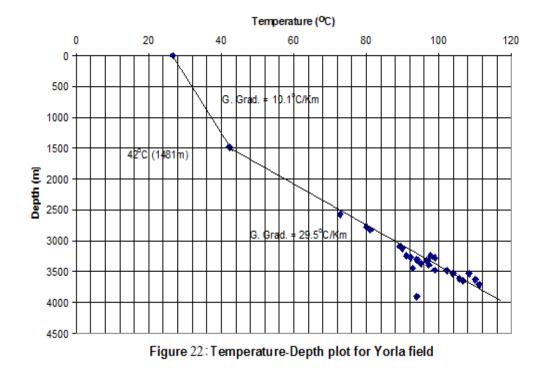
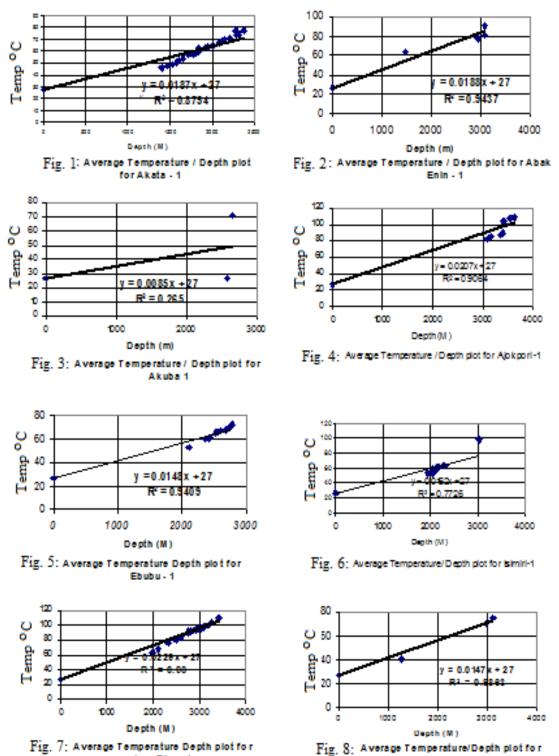


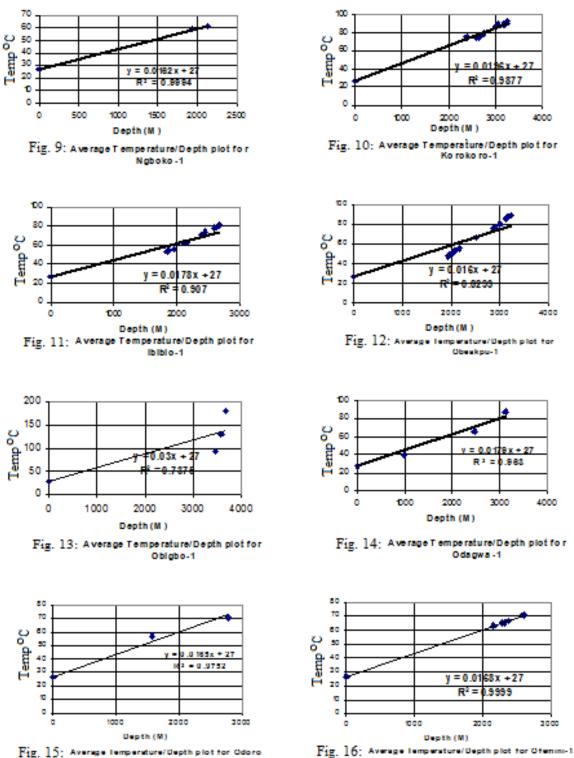
Figure 21: Temperature - Depth plot for Soku field

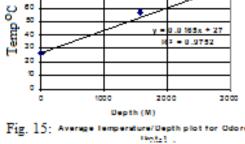


APPENDIX III



Imo River-1





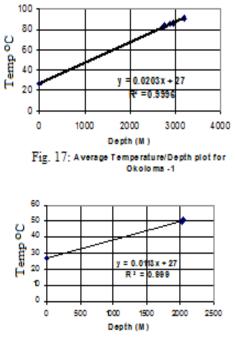
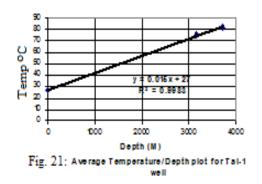


Fig. 19: Average Temperature/Depth plot for Oza-2



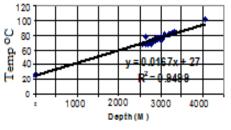


Fig. 23: Average Temperature/Depth plot for Ak2s0 - 4

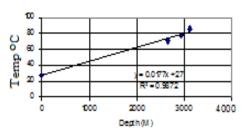


Fig. 18: Average Temperature Depth plot for Onne -1

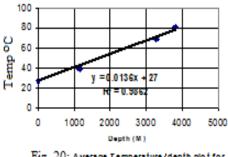


Fig. 20: A verage Temperature/depth plot for Tabangh -1

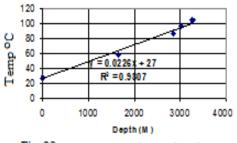
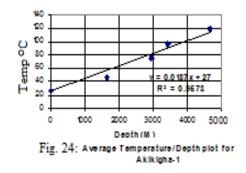


Fig. 22: Average Temperature/Depth plot for Akal -well



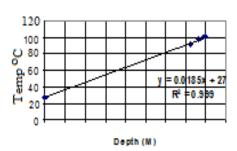


Fig. 25: Average Temperature/Depth plot forAlakiri - East -1

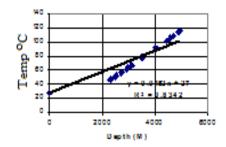


Fig. 27: Average Lenperature Depth plot for Awoba -

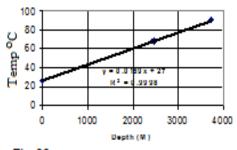
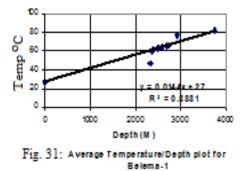
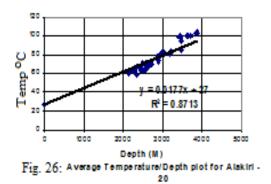


Fig. 29: Average Lemperature Depth plot for Baniele -1





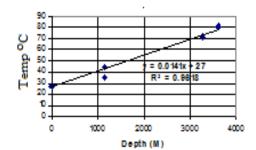


Fig. 28: Average Temperature/Depth plot for Bakana-1 well

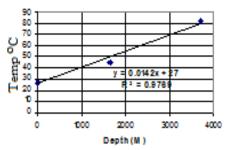


Fig.30: Average Temperature/Depth plot for Bille-1well

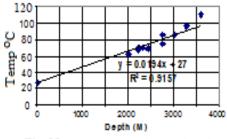


Fig. 32: Average Temperature/Depth plot for Bodo West -1

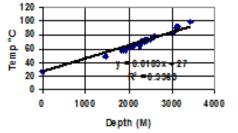
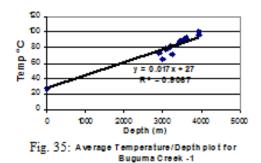
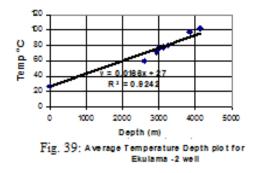


Fig. 33: Average Temperature/Depth plot for Bomu-1



120 100 ပ္စ္ဆ de e = 0.018 x + 27 R² = 0.8827 40 20 0 4000 0 1000 2000 3000 5000 Depth (m)

Fig. 37: Average Temperature Depth plot for Choble -1



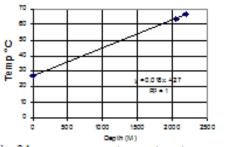


Fig. 34: Average Temperature/Depth plot for Bonny North - 1

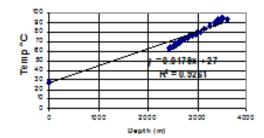


Fig. 36: Average Temperature Depth plot for Cawthorne Channel -1

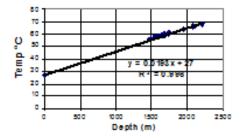


Fig. 38: Average Temperature Depth plot for Ekim -2 well

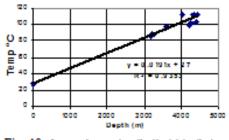
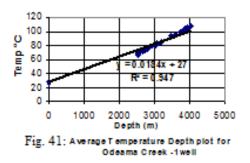


Fig. 40: A verse l'emperature Depth plot for Krakama -



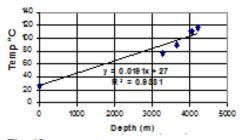


Fig. 42: A verage Temperature Depth plot for Ogu - 1 well

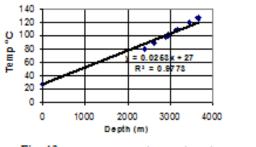


Fig. 43: Average Temperature Depth plot for Opobo South well

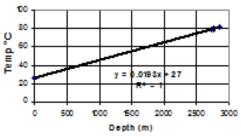
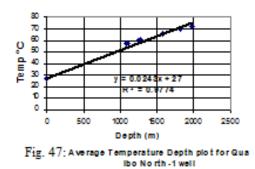


Fig. 45: Average Temperature Depth plot for Otak lk po -1 well



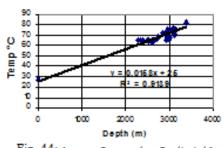


Fig. 44: A verage Temperature Depth plot for Orubiri - 1 well

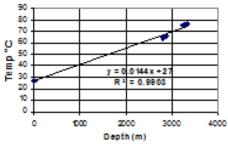
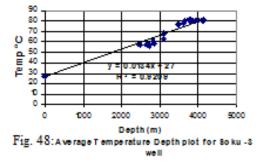


Fig. 46:



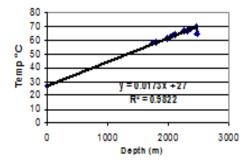
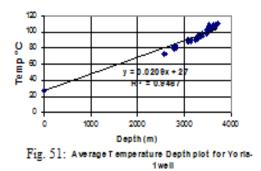


Fig. 49: Average Temperature Depth plot for Uquo - 2



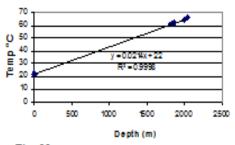
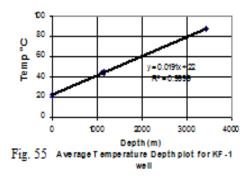


Fig. 53: Average Lemperature D epth plot for Kappe - 1 well



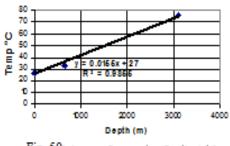


Fig. 50: Average Temperature Depth plot for Yomene -1 well

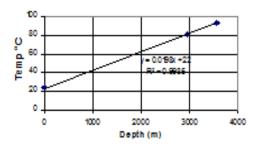


Fig. 52: A verage Temperature Depth plot for Koronama -1 well

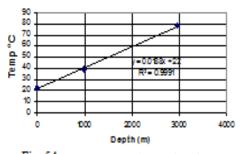
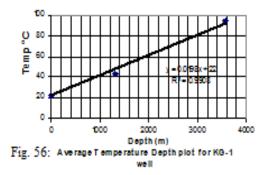


Fig. 54: A verage Temperature Depth plot for KR-1 well



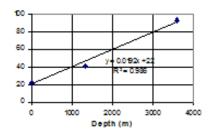


Fig. 57: Average Lemperature Depth plot for KH-1 well

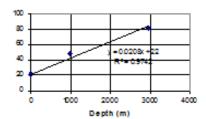


Fig. 59: A verage T emperature Depth plot for KQ-1 well

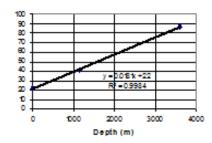


Fig. 61: A verage T emperature Depth plot for JA-1 well

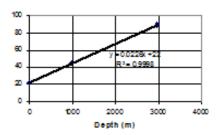


Fig. 63: Average Temperature Depth plot for JK-1 well

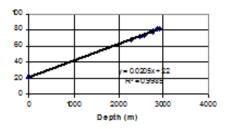


Fig. 58: Average Temperature Depth plot for KD-1 well

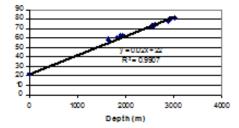


Fig. 60; Average Temperature Depth plot for KL-1 well

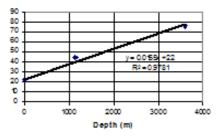


Fig. 62: A verage T emperature Depth plot for JD-1 well

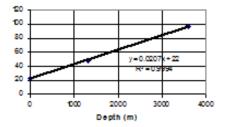


Fig. 64: A verage Temperature Depth plot for JN-1 well

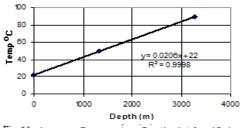


Fig. 65: A verage Temperature Depth plot for JO-1 well